Important note: For your information, there will be six problems in the midterm. One (15%) will be on the spectrum drawing (e.g., G(f), $G_+(f)$, $\tilde{G}(f)$, $\hat{G}(f)$, $\bar{S}_X(f)$, $\bar{S}_{\tilde{X}}(f)$, etc). Four (70%) will be from the sample problems. One (15%) will be from the slides (Up to 5-39).

Corrections

- Sample Problem 2(b) for Quiz 6: The last line of the solution should write, " $m'(t) = L_Q(f_m)\sin(2\pi f_m t) = \begin{cases} -\frac{f_m}{f_v}\sin(2\pi f_m t), & f_m \leq f_v \\ -\sin(2\pi f_m t), & f_m > f_v \end{cases}$.
- Sample Problem 3(c) for Quiz 6: The Hilbert transform of a constant is zero. Hence, $\mathcal{H}\left\{1 + \cos(2\pi f_0 t) + \cos^2(2\pi f_0 t) + \cos^3(2\pi f_0 t)\right\} = \frac{3}{2} + \frac{7}{4}\sin(2\pi f_0 t) + \frac{1}{2}\sin(2\pi (2f_0)t) + \frac{1}{4}\sin(2\pi (3f_0)t).$
- Slide 4-75: It should be " $J_n(\beta) \approx 0$ for $n \geq 2$."
- Slide 5-11: Remove "and coherent detection (observed at x(t))"
- Slide 5-12: Please remove the left-most "[" in " $[E[n^2(t)] = E[n_I^2(t)] = E[n_Q^2(t)]$."
- Slide 5-16: The third "=" should be " \approx ." In other words,

$$y(t) = \sqrt{(x^{2}(t))_{\text{LowPass}}}$$

= $\frac{1}{\sqrt{2}}\sqrt{[A_{c}(1+k_{a}m(t))+n_{I}(t)]^{2}+n_{Q}^{2}(t)}$
 $\approx \frac{1}{\sqrt{2}}[A_{c}(1+k_{a}m(t))+n_{I}(t)] \text{ if } A_{c}[1+k_{a}m(t)] \gg |\tilde{n}(t)|$

- Slide 5-21: It should be " $A_c[1 + k_a m(t)] \gg |\tilde{n}(t)|$."
- Slide 5-26: In two places, please change to $\sigma_N^2 = E[|\tilde{n}(t)|^2]$
- Slide 5-40: " $\phi(t) \phi(t)$ " should be " $\psi(t) \phi(t)$."

In what follows, the items leading with a \star are more important, and the items leading with two \star (i.e., $\star\star$) are the most important.

<u>Part I</u>

- 1-13 \sim 1-14 : Definition of stationarity and why we introduce stationarity
- \star 1-16 : Definition of autocorrelation function
- \star 1-17: Prove that the autocorrelation function becomes a function of time difference under stationarity.
- \star 1-19: Definition of autocovariance (given in the first line) and its relation with autocorrelation and mean functions (established at the bottom)

Prove that the autocorrelation function of a random process is equal to the sum of its autocovariance function and the product of its mean functions at the two time instances, i.e., $R_X(t_1, t_2) = C_X(t_1, t_2) + \mu_X(t_1)\mu_X^*(t_2)$.

- ****** 1-21: Definition of WSS (two conditions)
- 1-23: Definition of cyclostationarity
- ****** 1-24 ~ 1-25: Three important properties of WSS processes
- \star 1-28 \sim 1-42: Derivation of mean functions and autocorrelation functions (verification of WSS) for specific examples
- 1-43 and 1-44: Definition of cross-correlation function and correlation matrix
- 1-45 ~ 1-48: Derivation of cross-correlation function
- ****** 1-60 ~ 1-62 : Definition and example of a stable LTI system
- \star 1-63 and 1-65: Input-output relation of mean function and autocorrelation function for a stable LTI system
- ****** 1-66: Prove that in a stable LTI system, WSS input induces WSS output.

<u>Part II</u>

- 2-2: Formula of Fourier transform pair
- 2-3: Sufficient condition for the existence of Fourier transform (and inverse Fourier transform)
- 2-5 to 2-8: Definition of Dirac delta function and its properties
- 2-11: Fourier series

* 2-12 ~ 2-14: The proof of Poisson sum formula, i.e., $g_T(t) = \frac{1}{T} \sum_{n=-\infty}^{\infty} G\left(\frac{n}{T}\right) e^{j2\pi \frac{n}{T}t}$, where $g(t) = \begin{cases} g_T(t), & |t| < \frac{T}{2}; \\ 0, & \text{otherwise} \end{cases}$ is the generating function of a periodic function $g_T(t)$ with period T, and G(f) is the (Fourier) spectrum of g(t).

Proof: First, we note that

$$g_T(t) = \sum_{m=-\infty}^{\infty} g(t - mT).$$

Then, by Fourier series,

$$c_n = \frac{1}{T} \int_{-T/2}^{T/2} g_T(t) \exp\left(-j2\pi \frac{n}{T}t\right) dt$$
$$= \frac{1}{T} \int_{-T/2}^{T/2} g(t) \exp\left(-j2\pi \frac{n}{T}t\right) dt$$
$$= \frac{1}{T} G\left(\frac{n}{T}\right)$$

and

$$g_T(t) = \sum_{n=-\infty}^{\infty} c_n e^{j2\pi \frac{n}{T}t} = \frac{1}{T} \sum_{n=-\infty}^{\infty} G\left(\frac{n}{T}\right) e^{j2\pi \frac{n}{T}t}$$

- \star 2-19: Prove time-convolution \Leftrightarrow spectrum-multiplication.
- 2-26 and 2-29: Definitions of time-average autocorrelation and PSD, in particular

$$\bar{S}_X(f) = \lim_{T \to \infty} \frac{1}{2T} E[X(f) X_{2T}^*(f)]$$

- ****** 2-31 and 2-32: Input-output relation of (time-average) autocorrelation functions and (time-average) PSDs for a stable LTI filter
- ****** 2-38 to 2-43: Properties of PSD
- \star 2-44 ~ 2-49 and 2-58 ~ 2-59: Derivations of PSDs for specific examples
- \star 2-67 to 2-68: Definition and impracticability of white noise
- 2-79 and 2-81 : Definitions of null-to-null and rms bandwidth.
- 2-83 and 2-84 : Definition of noise equivalent bandwidth
- 2-86: Notion of time-bandwidth product

Part III

- $\star\star$ 3-5: Impulse response and transfer function of Hilbert transform
 - ★ 3-8 ~ 3-9: Prove that the Hilbert transform pairs are orthogonal to each other, where the inner product is defined as $\langle f(t), g(t) \rangle = \int_{-\infty}^{\infty} f(t)g^*(t)dt$.
 - ★ 3-12 to 3-13: Prove $g(t) = \operatorname{Re}\{g_+(t)\} = \operatorname{Re}\{\tilde{g}(t)\exp(j2\pi f_c t)\} = g_I(t)\cos(2\pi f_c t) g_Q(t)\sin(2\pi f_c t)$ based on their spectrum relations
 - 3-15 to 3-16: Canonical transmitter and receiver
 - 3-22: Show that Y(f) = H(f)X(f) implies $\tilde{Y}(f) = \frac{1}{2}\tilde{H}(f)\tilde{X}(f)$, where we define $H_+(f) = 2u(f)H(f)$ and $\tilde{H}(f) = H_+(f+f_c)$.
- $\star\star$ 3-26 to 3-29: Proofs of Properties 1 and 2
- ★★ 3-33: Proof of Property 7
- ** 3-34: Proof of $R_{N_I,N_Q}(0) = E[N_I(t)N_Q^*(t)] = 0$, i.e., $N_I(t)$ and $N_Q(t)$ are orthogonal. Note that this is true even if $N_I(t)$ and $N_Q(t)$ do not have zero means.
 - 3-35 and 3-38: Good to know the two properties
 - 3-46 and 3-50: Reyleigh distribution and Rician distribution
 - 3-53 to 3-55: Properties 6 and 6' of Bessel functions

Part IV

- ****** 4-5: DSB-C and overmodulation
- ****** 4-16 ~ 4-18: Envelop detector

- 4-21: Linear modulation
- ****** 4-22 and 4-23: Three kinds of linear modulations, which are DSB-C, SSB and VSB. In particular, you should know how to derive and draw their spectrums.
- $\star\star$ 4-25 and 4-26: Coherent receiver (Quadrature null effect of the coherent detector in 4-27)
 - 4-28: Costas receiver
- ★★ 4-31: SSB (energy gap requirement)
- ****** 4-35 and 4-37: VSB $M_{\text{VSB}}(f) = \frac{1}{2}M(f) j\frac{1}{2}H_Q(f)M(f)$
- 4-39: Recover M(f) from $M_{\text{VSB}}(f)$.
- ** 4-46: VSB $M_{\text{VSB}}(f) = \frac{1}{2}M(f) + j\frac{1}{2}M'(f)$, where $M'(f) = -H_Q(f)M(f)$
 - 4-53: Frequency translation
- 4-56: Angle modulation (PM and FM)
- ** 4-60: Instantaneous frequency, frequency deviation Δf and modulation index β of a single-tone FM
- ****** 4-66: Spectrum of Single-Tone FM and its relation with Bessel function (4-67 ~ 4-70)
- \star 4-79: Bandwidth of a General FM Wave based on Carson's rule
- \star 4-80 \sim 4-81 : Bandwidth of a General FM Wave based on universal curve
- ****** 4-86 ~ 4-93: Balanced frequency discriminator
- 4-95 ~ 4-96: FM Stereo Multiplexing
- 4-102 \sim 4-104: IF session and image interference

Part V

- $\star\star$ 5-4 \sim 5-6: Definitions of SNR_O, SNR_C and figure of merit
- $\star\star$ 5-8 \sim 5-13: Computations of SNR_O, SNR_C and figure of merit for DSB-C and coherent detector
- $\star\star$ 5-14 \sim 5-19: Computations of SNR_O, SNR_C and figure of merit for DSB-SC and envelop detector
- \star 5-20 \sim 5-23: Threshold effect of DSB-C and envelop detector (discussions in 5-34 and 5-35 are included)
- 5-24 \sim 5-33: Outside the scope of the midterm
- $\star\star$ 5-36 \sim 5-39: Derivation of the equivalent additive noise of FM and balanced frequency discriminator

- 1. For a single-tone FM transmission with $m(t) = A_m \cos(2\pi f_m t)$, we have $\Delta f = \beta f_m = k_f A_m$, where Δf is the frequency deviation, β is the modulation index, and k_f is the frequency sensitivity.
 - (a) Suppose $f_m = 15$ KHz. Give Δf if $\beta = 1.0, 2.0$ and 5.0.
 - (b) For the computation of transmission bandwidth, Carson's rule gives $B_{T,\text{Carson}} = 2\Delta f(1 + \frac{1}{\beta})$ and the universal curve transmission bandwidth $B_{T,\text{UC}}$ follows the below table:

β	$B_{T,\mathrm{UC}}/\Delta f$
0.1	20.0
0.3	13.3
0.5	8.0
1.0	6.0
2.0	4.0
5.0	3.2
10.0	2.8
20.0	2.5
30.0	2.3

Is $B_{T,\text{UC}} \geq B_{T,\text{Carson}}$ always true for a given Δf ?

Solution.

- (a) $\Delta f = 15, 30, 75$ KHz respectively for $\beta = 1.0, 2.0$ and 5.0
- (b) From $\frac{B_{T,\text{Carson}}}{\Delta f} = 2(1 + \frac{1}{\beta})$, we obtain

β	$B_{T,\mathrm{UC}}/\Delta f$	$B_{T,\mathrm{Carson}}/\Delta f$	2/eta
0.1	20.0	22.0	20.00
0.3	13.3	8.67	6.67
0.5	8.0	6.00	4.00
1.0	6.0	4.00	2.00
2.0	4.0	3.00	1.00
5.0	3.2	2.40	0.40
10.0	2.8	2.20	0.20
20.0	2.5	2.10	0.10
30.0	2.3	2.07	0.067

Therefore, when β is very small, we actually have $B_{T,UC} < B_{T,Carson}$.

2. The balanced frequency discriminator for an FM modulated signal $s(t) = \cos(2\pi f_c t + 2\pi k_f \int_0^t m(\tau) d\tau)$ is given below, where

$$H_1(f) = \begin{cases} j2\pi \left(f - f_c + \frac{B_T}{2} \right), & |f - f_c| \le \frac{B_T}{2} \\ j2\pi \left(f + f_c - \frac{B_T}{2} \right), & |f + f_c| \le \frac{B_T}{2} \\ 0, & \text{otherwise} \end{cases}$$

and

(a) The above block diagram can be transformed to its lowpass equivalent diagram with

$$\begin{cases} \tilde{s}(t) = \exp\left(j2\pi k_f \int_0^t m(\tau)d\tau\right) \\ \tilde{s}_1(t) = j\pi B_T \tilde{s}(t) + \frac{d\tilde{s}(t)}{dt} \\ \tilde{s}_2(t) = j\pi B_T \tilde{s}(t) - \frac{d\tilde{s}(t)}{dt} \end{cases}$$

as:

s



Show that

$$\tilde{s}_1(t) = j\pi B_T \left(1 + \frac{2k_f}{B_T}m(t)\right)\tilde{s}(t)$$

and

$$\tilde{s}_2(t) = j\pi B_T \left(1 - \frac{2k_f}{B_T}m(t)\right)\tilde{s}(t).$$

Note: We set a = 1 in the formula of $H_1(f)$ and $H_2(f)$ for analytical convenience.

- (b) Further, represent $|\tilde{s}_1(t)|$ and $|\tilde{s}_2(t)|$ as a function of m(t).
- (c) Find the sufficient and necessary condition for the validity of $\tilde{s}_o(t) = 4\pi k_f m(t)$.

Solution.

(a) By noting that

$$\frac{d\tilde{s}(t)}{dt} = \frac{d\left(j2\pi k_f \int_0^t m(\tau)d\tau\right)}{dt} \cdot e^{j2\pi k_f \int_0^t m(\tau)d\tau} = j2\pi k_f m(t)\tilde{s}(t),$$

we derive

$$\tilde{s}_{1}(t) = j\pi B_{T}\tilde{s}(t) + \frac{d\tilde{s}(t)}{dt}$$

$$= j\pi B_{T}\tilde{s}(t) + j2\pi k_{f}m(t)\tilde{s}(t)$$

$$= j\pi B_{T}\left(1 + \frac{2k_{f}}{B_{T}}m(t)\right)\tilde{s}(t)$$

and

$$\tilde{s}_{2}(t) = j\pi B_{T}\tilde{s}(t) - \frac{d\tilde{s}(t)}{dt}$$

$$= j\pi B_{T}\tilde{s}(t) - j2\pi k_{f}m(t)\tilde{s}(t)$$

$$= j\pi B_{T}\left(1 - \frac{2k_{f}}{B_{T}}m(t)\right)\tilde{s}(t).$$

(b)

$$\begin{aligned} |\tilde{s}_1(t)| &= \left| j\pi B_T \left(1 + \frac{2k_f}{B_T} m(t) \right) \tilde{s}(t) \right| \\ &= \left| j\pi B_T \right| \left| 1 + \frac{2k_f}{B_T} m(t) \right| \left| \tilde{s}(t) \right| \\ &= \left| \pi B_T \right| 1 + \frac{2k_f}{B_T} m(t) \right| \end{aligned}$$

and similarly

$$|\tilde{s}_2(t)| = \pi B_T \left| 1 - \frac{2k_f}{B_T} m(t) \right|.$$

(c) $\left|\frac{2k_f}{B_T}m(t)\right| \le 1$, i.e., $|m(t)| \le \frac{B_T}{2k_f}$.

3. (a) Show that the SNR_C of the DSB-SC transmission (See the figure below) is equal to

$$\mathrm{SNR}_{\mathrm{C}} = \frac{P}{2WN_0},$$

where $s(t) = m(t) \cos(2\pi f_c t)$, m(t) is a zero-mean WSS process with $E[m^2(t)] = P$ and with bandwidth W, and w(t) is an additive white Gaussian noise with two-sided PSD $N_0/2$.



- (b) Continue from (a). Find the SNR_O of the DSB-SC transmission.
 Hint: You need to find the expression of the final output y(t). Then, SNR_O is the average power of the signal content in y(t) divided by the average power of the noise content in y(t).
- (c) Show that the SNR_C of the DSB-C transmission (See the figure below) is equal to

$$\mathrm{SNR}_{\mathrm{C}} = \frac{1 + k_a^2 P}{2W N_0},$$

where $s(t) = [1+k_a m(t)] \cos(2\pi f_c t)$, m(t) is a zero-mean WSS process with $E[m^2(t)] = P$ and with bandwidth W, and w(t) is an additive white Gaussian noise with two-sided PSD $N_0/2$.



(d) Show that under fixed N_0 , the SNR_C of DSB-C is bounded due to the constraint $|k_a m(t)| \leq 1$, while the SNR_C of DSB-SC grows linearly with P. Note: Hence, from the standpoint of "forms of marit" the reference target (i.e., SNR).

Note: Hence, from the standpoint of "figure of merit," the reference target (i.e., SNR_C) of DSB-C is actually "worse" than the reference target of DSB-SC as P is moderately large.

Solution.

(a) For the computation of SNR_C , we first obtain the **averaged signal power** (in the time-averaged form as s(t) is not necessarily WSS):

$$\lim_{T \to \infty} \frac{1}{2T} \int_{-T}^{T} E[s^{2}(t)] dt = \lim_{T \to \infty} \frac{1}{2T} \int_{-T}^{T} E[m^{2}(t) \cos^{2}(2\pi f_{c}t)] dt$$

$$= \lim_{T \to \infty} \frac{1}{2T} \int_{-T}^{T} E[m^{2}(t)] \cos^{2}(2\pi f_{c}t) dt$$

$$= \lim_{T \to \infty} \frac{1}{2T} \int_{-T}^{T} P \cos^{2}(2\pi f_{c}t) dt$$
Because $m(t)$ is WSS and $E[m^{2}(t)] = P$

$$= \lim_{T \to \infty} \frac{P}{4T} \int_{-T}^{T} [1 + \cos(4\pi f_{c}t)] dt$$

$$= \frac{P}{2},$$

where

$$\frac{1}{2T} \int_{-T}^{T} \cos(4\pi f_c t) dt = \left. \frac{1}{8\pi f_c T} \sin(4\pi f_c t) \right|_{-T}^{T} = \frac{\sin(4\pi f_c T)}{4\pi f_c T} \to 0 \text{ as } T \to \infty.$$

The noise power in the message bandwidth is given by

$$\int_{-W}^{W} S_w(f) df = \int_{-W}^{W} \frac{N_0}{2} df = W N_0.$$

Therefore,

$$\mathrm{SNR}_{\mathrm{C}} = \frac{P/2}{WN_0} = \frac{P}{2WN_0}.$$

(b) The functional blocks give the following equations:

$$\begin{cases} s(t) = m(t)\cos(2\pi f_c t) \\ x(t) = s(t) + n(t) \\ \text{where } n(t) = n_I(t)\cos(2\pi f_c t) - n_Q(t)\sin(2\pi f_c t) \text{ is the filtered white noise} \\ v(t) = x(t)\cos(2\pi f_c t) \\ y(t) = v(t) \text{ passing through an ideal lowpass filter} \\ \Rightarrow \begin{cases} v(t) = [m(t)\cos(2\pi f_c t) + n(t)]\cos(2\pi f_c t) \\ y(t) = v(t) \text{ passing through an ideal lowpass filter} \\ \Rightarrow y(t) = [m(t)\cos^2(2\pi f_c t)]_{\text{Lowpass}} + [n_I(t)\cos^2(2\pi f_c t) - n_Q(t)\sin(2\pi f_c t)\cos(2\pi f_c t)]_{\text{Lowpass}} \\ \Rightarrow \boxed{y(t) = \frac{1}{2}m(t) + \frac{1}{2}n_I(t)} \end{cases}$$

$$\Rightarrow \text{SNR}_{\text{O,DSB-SC}} = \frac{E[A_c^2 m^2(t)/4]}{E[n_I^2(t)/4]} = \frac{A_c^2 P}{E[n^2(t)]} = \frac{A_c^2 P}{2W N_0}$$

(c)

$$\lim_{T \to \infty} \frac{1}{2T} \int_{-T}^{T} E[s^{2}(t)] dt = \lim_{T \to \infty} \frac{1}{2T} \int_{-T}^{T} E[(1+k_{a}m(t))^{2} \cos^{2}(2\pi f_{c}t)] dt$$

$$= \lim_{T \to \infty} \frac{1}{2T} \int_{-T}^{T} E[(1+k_{a}m(t))^{2}] \cos^{2}(2\pi f_{c}t) dt$$

$$= \lim_{T \to \infty} \frac{1}{2T} \int_{-T}^{T} (1+k_{a}^{2}P) \cos^{2}(2\pi f_{c}t) dt$$
Because $m(t)$ is zero-mean WSS and $E[m^{2}(t)] = P$

$$= \lim_{T \to \infty} \frac{(1+k_{a}^{2}P)}{4T} \int_{-T}^{T} [1+\cos(4\pi f_{c}t)] dt$$

$$= \frac{(1+k_{a}^{2}P)}{2},$$

where

$$\frac{1}{2T} \int_{-T}^{T} \cos(4\pi f_c t) dt = \frac{1}{8\pi f_c T} \sin(4\pi f_c t) \Big|_{-T}^{T} = \frac{\sin(4\pi f_c T)}{4\pi f_c T} \to 0 \text{ as } T \to \infty.$$

The noise power in the message bandwidth is given by

$$\int_{-W}^{W} S_w(f) df = \int_{-W}^{W} \frac{N_0}{2} df = W N_0.$$

Therefore,

$$SNR_C = \frac{(1+k_a^2 P)/2}{WN_0} = \frac{1+k_a^2 P}{2WN_0}.$$

(d) $|k_a m(t)| \leq 1$ implies $k_a^2 m^2(t) \leq 1$, which in turn implies $E[k_a^2 m^2(t)] = k_a^2 P \leq 1$. Therefore,

$$\mathrm{SNR}_{\mathrm{C},\mathrm{DSB-C}} = \frac{1+k_a^2 P}{2WN_0} \le \frac{1}{WN_0}.$$

This is in stark contrast to

$$SNR_{C, DSB-SC} = \frac{P}{2WN_0}$$

that grows linearly and unbounded with P.

Note: $SNR_{C,DSB-C}$ cannot be improved by growing P, not to mention its figure of merit is often much less than 1.

4. For an FM receiver below, we have $s(t) = A_c \cos(2\pi f_c t + \phi(t))$, where $\phi(t) = 2\pi k_f \int_0^t m(\tau) d\tau$. Denote the passband noise process (i.e., the noise process observed at the output of the bandpass filter) as

$$n(t) = n_I(t)\cos(2\pi f_c t) - n_Q(t)\sin(2\pi f_c t) = r(t)\cos(2\pi f_c t + \Psi(t)),$$

where $n_I(t) = r(t) \cos[\Psi(t)]$ and $n_Q(t) = r(t) \sin[\Psi(t)]$.



Due to the limiter, the amplitude of x(t) is of no influence on its output, and only the phase remains. Hence, we can assume the amplitude at the output of the limiter is 1 for simplicity. Show that the output of the limiter $x_{\text{limiter}}(t)$ is given by

$$x_{\text{limiter}}(t) = \cos[2\pi f_c t + \theta(t)]$$

where

$$\theta(t) = \phi(t) + \tan^{-1} \left(\frac{r(t) \sin[\Psi(t) - \phi(t)]}{A_c + r(t) \cos[\Psi(t) - \phi(t)]} \right).$$

Hint: For simplicity during derivation, you can denote $A = 2\pi f_c t + \phi(t)$ and $B = \Psi(t) - \phi(t)$ and complete the following derivation:

$$\begin{aligned} x(t) &= A_c \cos[2\pi f_c t + \phi(t)] + r(t) \cos[2\pi f_c t + \Psi(t)] \\ &= A_c \cos[2\pi f_c t + \phi(t)] + r(t) \cos[2\pi f_c t + \phi(t)] + \Psi(t) - \phi(t)] \\ &= A_c \cos(\mathbf{A}) + r(t) \cos(\mathbf{A} + \mathbf{B}) \\ &= \cdots \end{aligned}$$

Solution. Denoting $A = 2\pi f_c t + \phi(t)$ and $B = \Psi(t) - \phi(t)$, we obtain

$$\begin{split} x(t) &= A_c \cos(\mathbf{A}) + r(t) \cos(\mathbf{A} + \mathbf{B}) \\ &= A_c \cos(\mathbf{A}) + r(t) \cos(\mathbf{A}) \cos(\mathbf{B}) - r(t) \sin(\mathbf{A}) \sin(\mathbf{B}) \\ &= [A_c + r(t) \cos(\mathbf{B})] \cos(\mathbf{A}) - r(t) \sin(\mathbf{B}) \sin(\mathbf{A}) \\ &= \sqrt{[A_c + r(t) \cos(\mathbf{B})]^2 + [r(t) \sin(\mathbf{B})]^2} \\ &\times \left(\frac{[A_c + r(t) \cos(\mathbf{B})]^2 + [r(t) \sin(\mathbf{B})]^2}{\sqrt{[A_c + r(t) \cos(\mathbf{B})]^2 + [r(t) \sin(\mathbf{B})]^2}} \cos(\mathbf{A}) \\ &- \frac{r(t) \sin(\mathbf{B})}{\sqrt{[A_c + r(t) \cos(\mathbf{B})]^2 + [r(t) \sin(\mathbf{B})]^2}} \sin(\mathbf{A}) \right) \\ &= \sqrt{[A_c + r(t) \cos(\mathbf{B})]^2 + [r(t) \sin(\mathbf{B})]^2} (\cos(\phi_{\text{noise}}(t)) \cos(\mathbf{A}) - \sin(\phi_{\text{noise}}(t)) \sin(\mathbf{A})) \\ &= \cos(\mathbf{A} + \phi_{\text{noise}}(t)), \end{split}$$

where

$$\phi_{\text{noise}}(t) = \tan^{-1} \left(\frac{r(t)\sin(B)}{A_c + r(t)\cos(B)} \right).$$