
Part 3 Hilbert Transform and Canonical Representation of Signals

Hilbert Transform

- How to obtain $g_+(t)$?
- Answer: *Hilbert Transformer*.

Proof: Observe that

$$2u(f) = 1 + \text{sgn}(f), \text{ where } \text{sgn}(f) = \begin{cases} 1, & f > 0 \\ 0, & f = 0 \\ -1, & f < 0 \end{cases}$$

Then by the next slide, we learn that

$$2u(f) \xrightarrow{\text{Inverse Fourier}} \delta(t) + j \frac{1}{\pi t} \cdot \mathbf{1}\{t \neq 0\}$$

By extended Fourier transform,

$$\begin{aligned}
 \int_{-\infty}^{\infty} \text{sgn}(f) e^{-a|f|+j2\pi ft} df &= \int_0^{\infty} e^{-a|f|+j2\pi ft} df - \int_{-\infty}^0 e^{-a|f|+j2\pi ft} df \\
 &= \int_0^{\infty} e^{-(a-j2\pi t)f} df - \int_{-\infty}^0 e^{(a+j2\pi t)f} df \\
 &= \frac{1}{a-j2\pi t} - \frac{1}{a+j2\pi t} \\
 &= \frac{j4\pi t}{a^2+4\pi^2 t^2}
 \end{aligned}$$

$$\text{sgn}(f) \xrightarrow{\text{InverseFourier}} \lim_{a \downarrow 0} j \frac{4\pi t}{a^2+4\pi^2 t^2} = \begin{cases} \frac{j}{\pi t}, & t \neq 0 \\ 0, & t = 0 \end{cases}$$

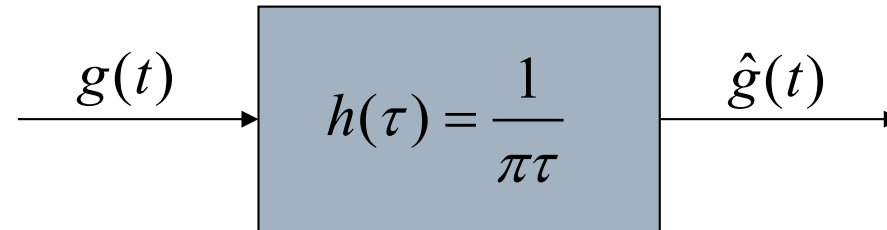
$$2u(f) = 1 + \text{sgn}(f) \xrightarrow{\text{InverseFourier}} \delta(t) + \frac{j}{\pi t} \cdot \mathbf{1}\{t \neq 0\}$$

Hilbert Transform

$$\begin{aligned}g_+(t) &= \text{Fourier}^{-1}\{2u(f)G(f)\} \\ &= \text{Fourier}^{-1}\{2u(f)\} * \text{Fourier}^{-1}\{G(f)\} \\ &= \left(\delta(t) + j \frac{1}{\pi t} \cdot \mathbf{1}\{t \neq 0\} \right) * g(t) \\ &= g(t) + j \frac{1}{\pi t} \cdot \mathbf{1}\{t \neq 0\} * g(t) \\ &= g(t) + j\hat{g}(t),\end{aligned}$$

where $\hat{g}(t) = \int_{-\infty}^{\infty} \frac{g(\tau)}{\pi(t-\tau)} d\tau$ is named the Hilbert Transform of $g(t)$.

Hilbert Transform

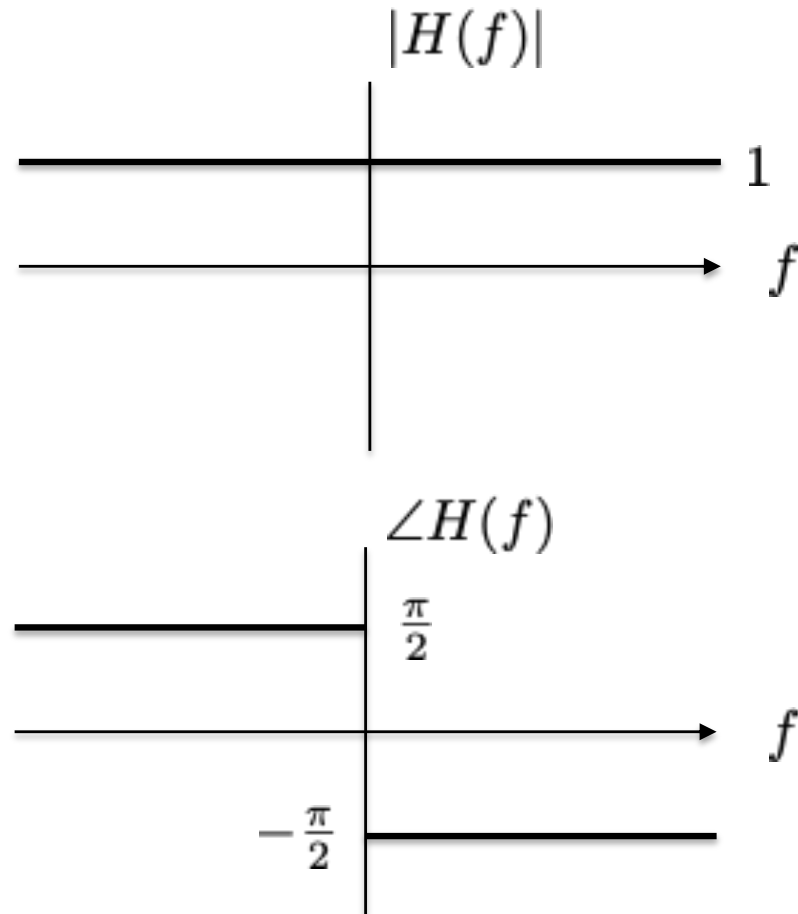


$$h(\tau) = \frac{1}{\pi\tau} \xrightarrow{\text{Fourier}} H(f) = -j \operatorname{sgn}(f), \text{ where } \operatorname{sgn}(f) = \begin{cases} 1, & f > 0 \\ 0, & f = 0 \\ -1, & f < 0 \end{cases}$$

$$\Rightarrow \hat{G}(f) = -j \operatorname{sgn}(f) \cdot G(f) = \begin{cases} |G(f)| \exp\{j[\angle G(f) - \pi/2]\}, & f > 0 \\ 0, & f = 0 \\ |G(f)| \exp\{j[\angle G(f) + \pi/2]\}, & f < 0 \end{cases}$$

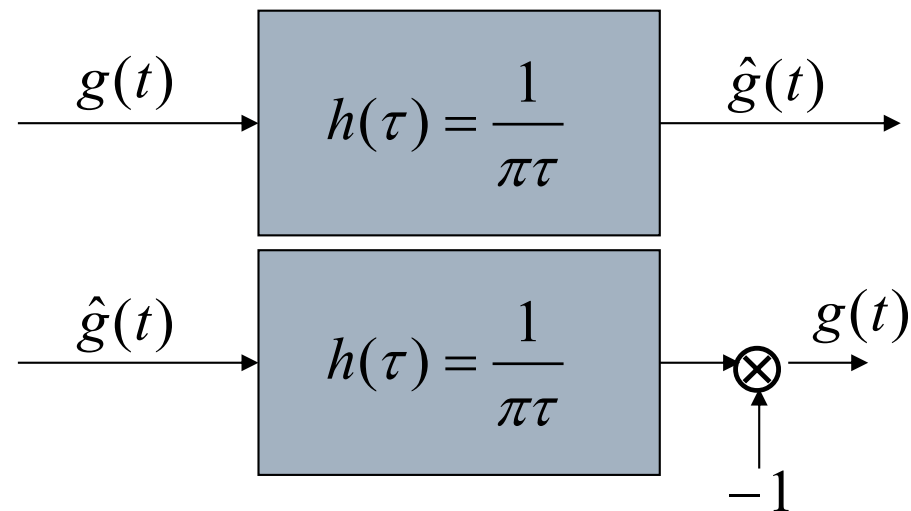
Hilbert Transform

- Hence, Hilbert Transform is basically a *90 degree phase shifter*.



Hilbert Transform

$$\text{Hilbert Transform Pair} \begin{cases} \hat{g}(t) = \frac{1}{\pi} \int_{-\infty}^{\infty} \frac{g(\tau)}{t - \tau} d\tau \\ g(t) = -\frac{1}{\pi} \int_{-\infty}^{\infty} \frac{\hat{g}(\tau)}{t - \tau} d\tau \end{cases}$$



Hilbert Transform

- An important property of Hilbert Transform is that:

$g(t)$ and $\hat{g}(t)$ are orthogonal in the sense of Integration.

In other words, $\int_{-\infty}^{\infty} g(t)\hat{g}(t)dt = 0$.

(See the proof in the next slide.)

The real and imaginary parts of $g_+(t) = g(t) + j\hat{g}(t)$ are orthogonal to each other.

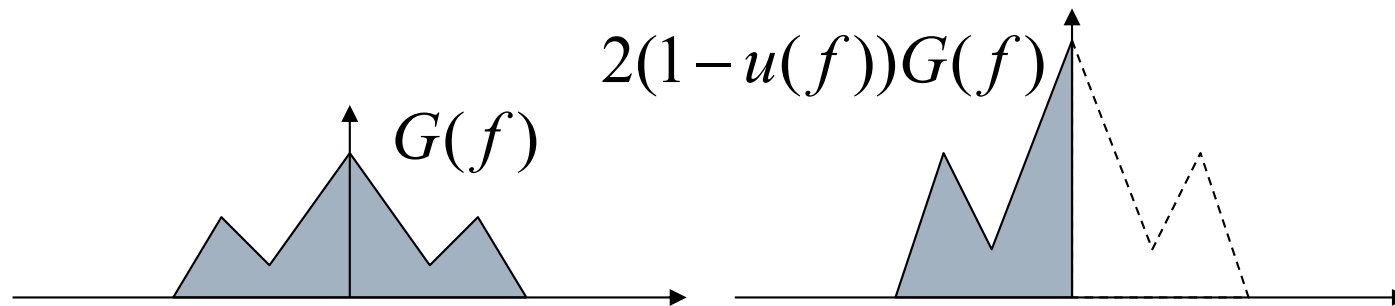
(Examples of Hilbert Transform Pairs can be found in Table A6.4.)

$$\begin{aligned}
\int_{-\infty}^{\infty} g(t)\hat{g}(t)dt &= \int_{-\infty}^{\infty} g(t)\left(\int_{-\infty}^{\infty} \hat{G}(f)e^{j2\pi ft}df\right)dt \\
&= \int_{-\infty}^{\infty} \hat{G}(f)\left(\int_{-\infty}^{\infty} g(t)e^{j2\pi ft}dt\right)df \\
&= \int_{-\infty}^{\infty} \hat{G}(f)G(-f)df \\
&= -j\int_{-\infty}^{\infty} \text{sgn}(f)G(f)G(-f)df \\
&= -j\left(\int_0^{\infty} G(f)G(-f)df - \int_{-\infty}^0 G(f)G(-f)df\right) \\
&= -j\left(\int_0^{\infty} G(f)G(-f)df - \int_0^{\infty} G(-f)G(f)df\right) \\
&= 0, \text{ if } \int_0^{\infty} G(f)G(-f)df < \infty.
\end{aligned}$$

Complex Representation of Signals and Systems

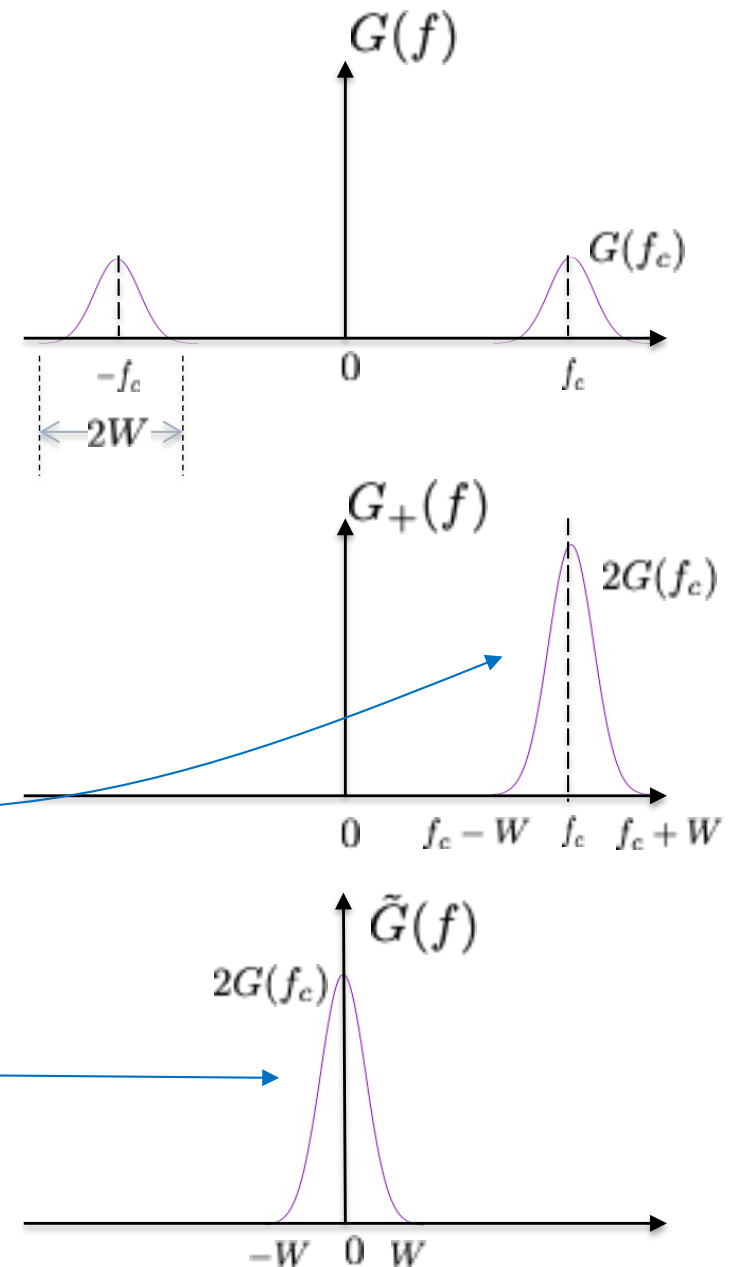
- $g_+(t)$ is named the *pre-envelope*, or *analytical signal*, of $g(t)$.
- We can similarly define

$$g_-(t) = g(t) - j\hat{g}(t)$$



Canonical Representation of Bandpass Signals

- Now let $G(f)$ be a *narrow-band signal* for which $2W \ll f_c$.
- Then we can obtain its pre-envelope $G_+(f)$.
- Afterwards, we can shift the pre-envelope to its low-pass signal $\tilde{G}(f) = G_+(f + f_c)$



Canonical Representation of Bandpass Signal

- These steps give the relation between the complex *lowpass signal* (baseband signal) and the real *bandpass signal* (passband signal).

$$g(t) = \text{Re}\{g_+(t)\} = \text{Re}\{\tilde{g}(t) \exp(j2\pi f_c t)\}$$

- Quite often, the real and imaginary parts of complex lowpass signal are respectively denoted by $g_I(t)$ and $g_Q(t)$.

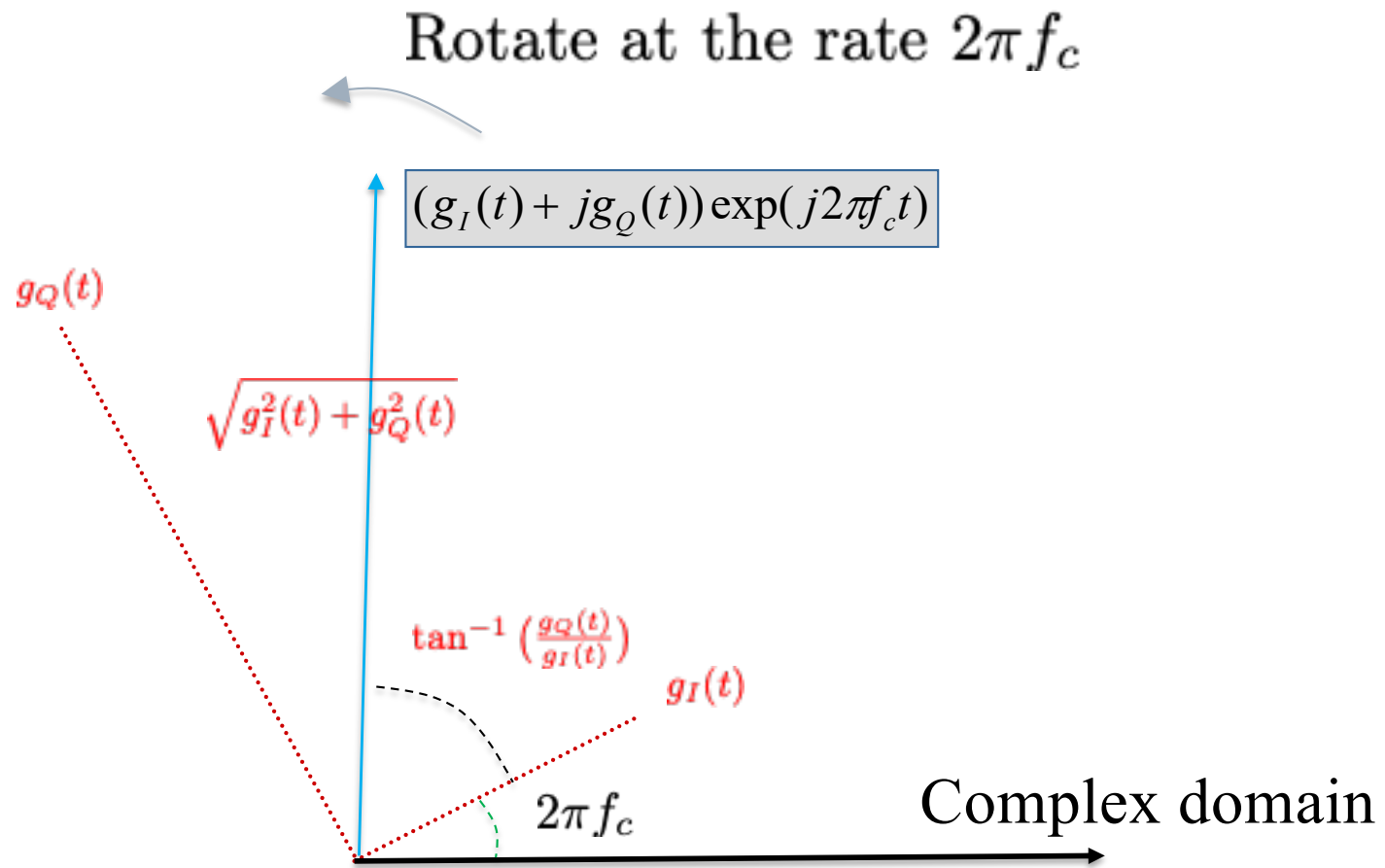
Canonical Representation of Bandpass Signal

□ In terminology,

$$\left\{ \begin{array}{ll} g_+(t) & \text{pre - envelope} \\ \tilde{g}(t) & \text{complex envelope} \\ g_I(t) & \text{in - phase component of the band - pass signal } g(t) \\ g_Q(t) & \text{quadrature component of the band - pass signal } g(t) \end{array} \right.$$

This leads to a *canonical*, or *standard*, expression for $g(t)$.

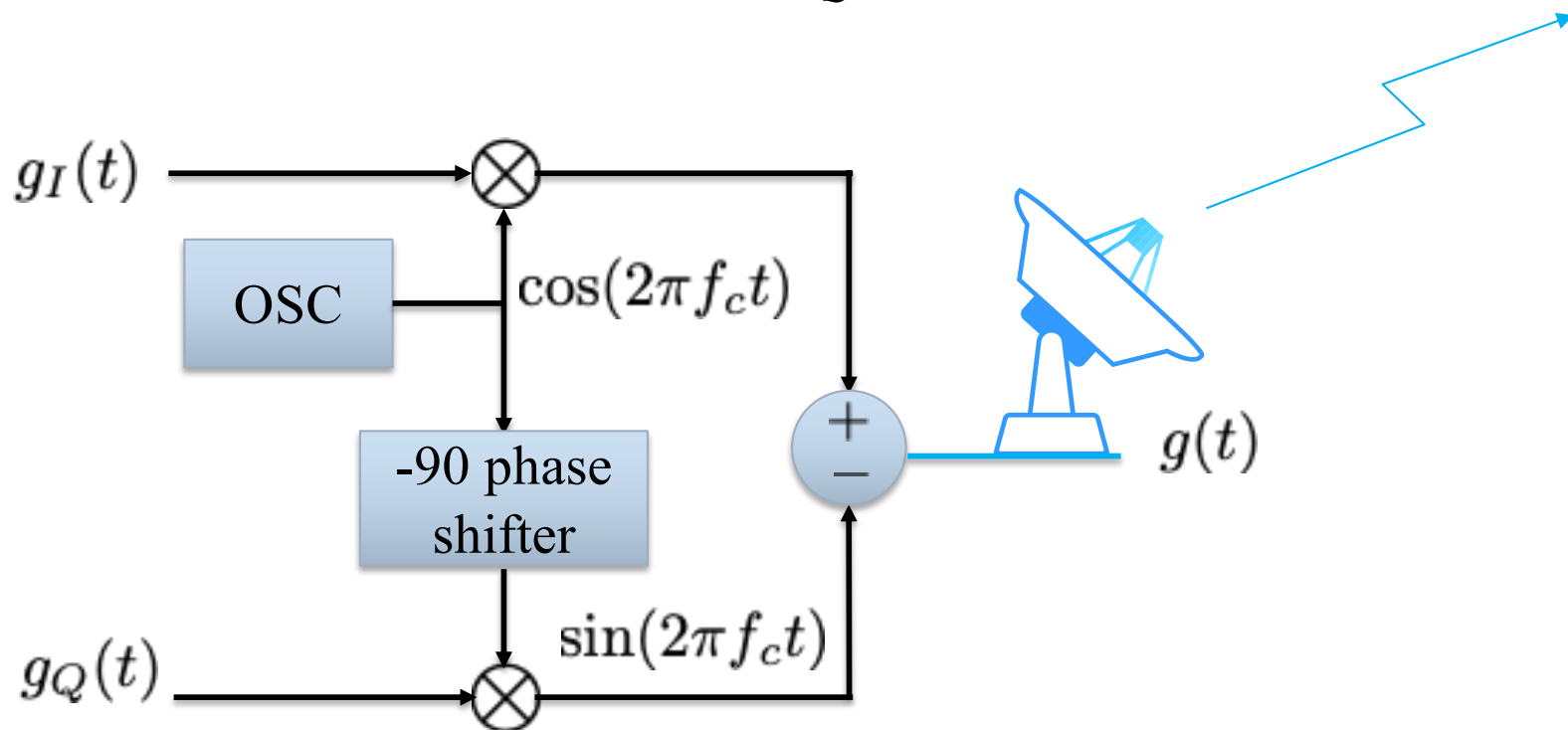
$$\begin{aligned} g(t) &= \text{Re} \left\{ (g_I(t) + jg_Q(t)) \exp(j2\pi f_c t) \right\} \\ &= g_I(t) \cos(2\pi f_c t) - g_Q(t) \sin(2\pi f_c t) \end{aligned}$$



Canonical Representation of Bandpass Signal

□ Canonical transmitter

$$g(t) = g_I(t) \cos(2\pi f_c t) - g_Q(t) \sin(2\pi f_c t)$$

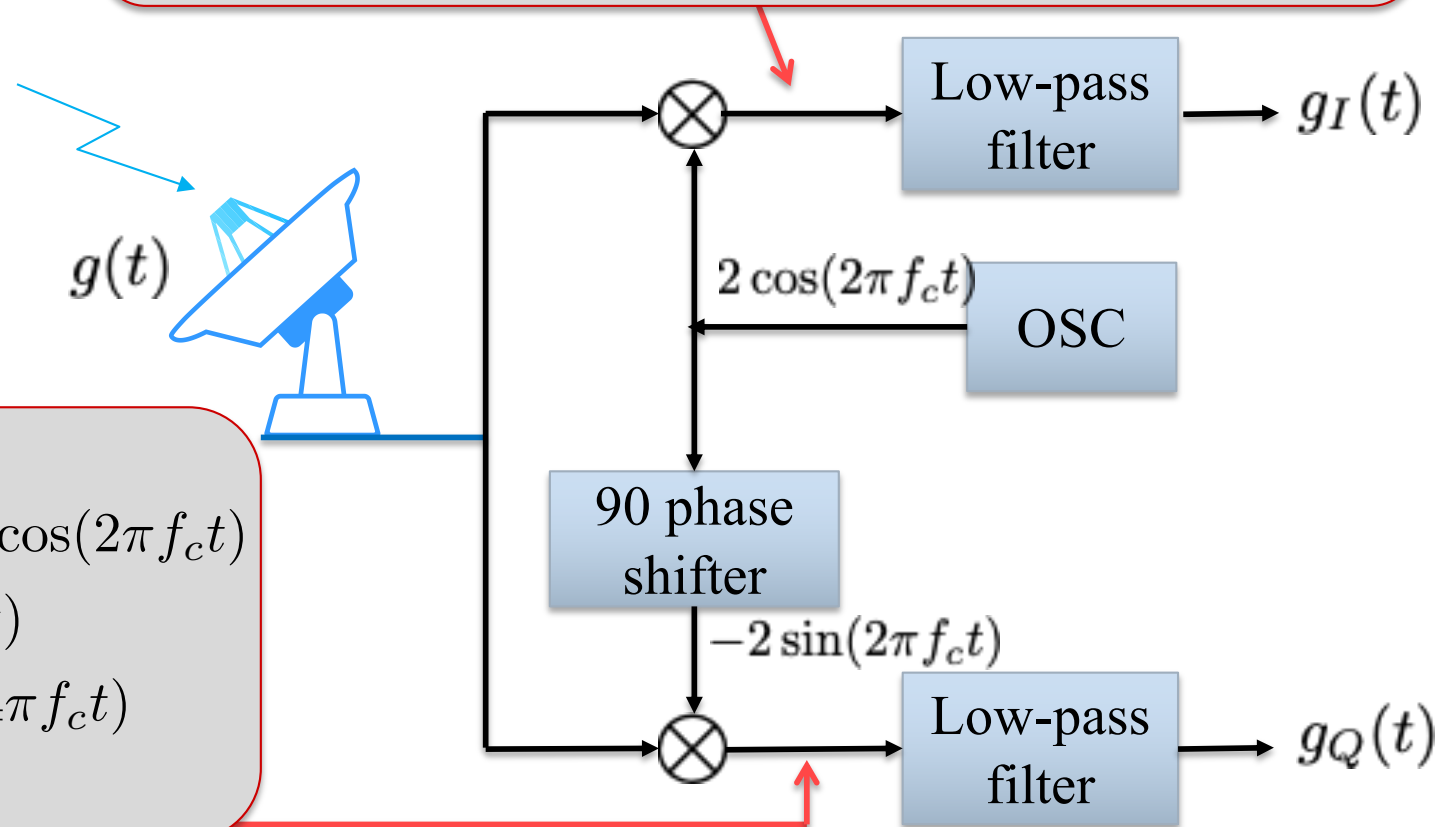


Canonical Representation of Bandpass Signal

Canonical receiver

$$\begin{aligned}
 & 2g(t) \cos(2\pi f_c t) \\
 = & 2g_I(t) \cos^2(2\pi f_c t) - 2g_Q(t) \sin(2\pi f_c t) \cos(2\pi f_c t) \\
 = & g_I(t) + g_I(t) \cos(4\pi f_c t) - g_Q(t) \sin(4\pi f_c t)
 \end{aligned}$$

$$\begin{aligned}
 & -2g(t) \sin(2\pi f_c t) \\
 = & -2g_I(t) \sin(2\pi f_c t) \cos(2\pi f_c t) \\
 & + 2g_Q(t) \sin^2(2\pi f_c t) \\
 = & g_Q(t) - g_Q(t) \cos(4\pi f_c t) \\
 & - g_I(t) \sin(4\pi f_c t)
 \end{aligned}$$



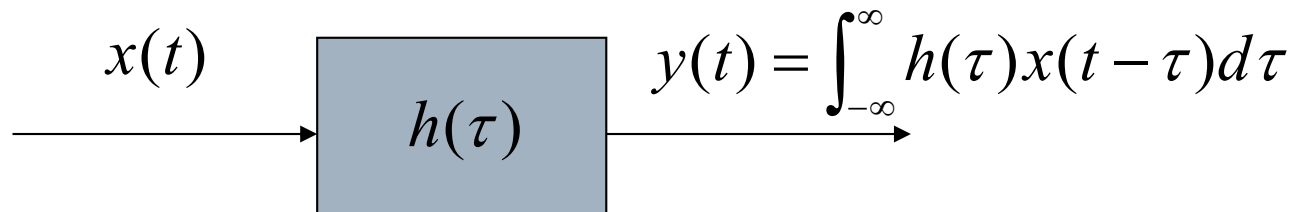
More Terminology

$g_+(t)$	pre - envelope
$\tilde{g}(t)$	complex envelope
$g_I(t)$	in - phase component of the band - pass signal $g(t)$
$g_Q(t)$	quadrature component of the band - pass signal $g(t)$

$$\left\{ \begin{array}{l} a(t) = |g_+(t)| = |\tilde{g}(t)| = \sqrt{g_I^2(t) + g_Q^2(t)} \\ \text{natural envelope or envelope of } g(t) \\ \phi(t) = \tan^{-1} \left(\frac{g_Q(t)}{g_I(t)} \right) \text{ phase of } g(t) \end{array} \right.$$

Bandpass System

- Consider the case of passing a bandpass signal $x(t)$ through a real LTI filter $h(\tau)$ to yield an output $y(t)$.



- Can we have a *lowpass equivalent system* for the bandpass system?

□ Similar to the previous analysis, we have:

Assumption : The spectrum of $x(t)$ is limited to within $\pm W$ Hz of the carrier frequency f_c , and $W < f_c$.

$$\begin{cases} x(t) = \text{Re}\left\{ \tilde{x}(t)e^{j2\pi f_c t} \right\} = x_I(t)\cos(2\pi f_c t) - x_Q(t)\sin(2\pi f_c t) \\ \tilde{x}(t) = x_I(t) + jx_Q(t) \end{cases}$$

Assumption : The spectrum of $h(\tau)$ is limited to within $\pm B$ Hz of the carrier frequency f_c , and $B < f_c$.

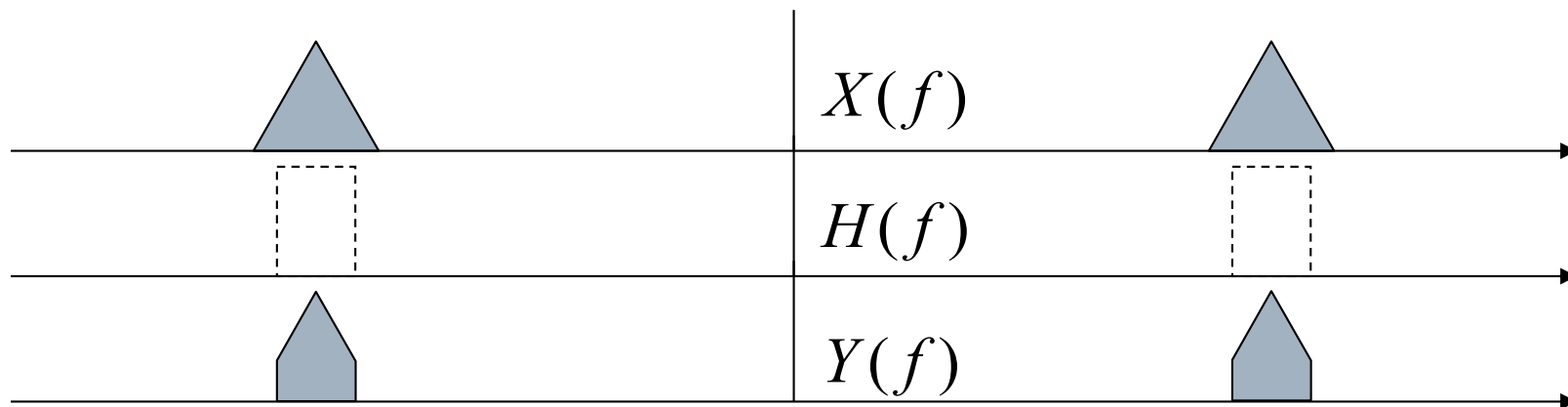
$$\begin{cases} h(\tau) = \text{Re}\left\{ \tilde{h}(\tau)e^{j2\pi f_c \tau} \right\} = h_I(\tau)\cos(2\pi f_c \tau) - h_Q(\tau)\sin(2\pi f_c \tau) \\ \tilde{h}(\tau) = h_I(\tau) + jh_Q(\tau) \quad \text{complex impulse response} \end{cases}$$

□ Now, is the filter output $y(t)$ also a bandpass signal?

$$Y(f) = X(f)H(f)$$

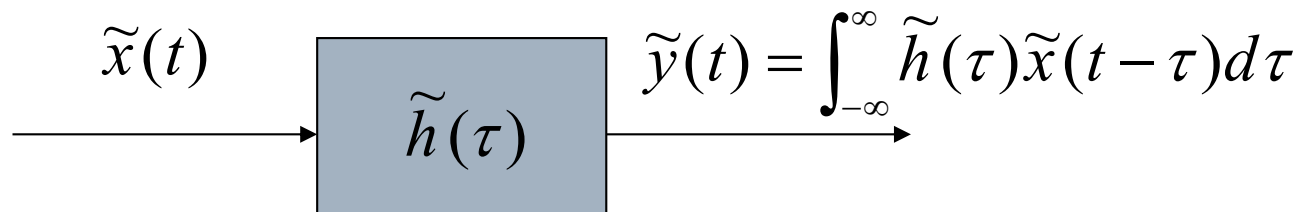
⇒ The spectrum of $y(t)$ is limited to within $\pm \min\{W, B\}$ Hz of the carrier frequency f_c , provided that $\max\{W, B\} < f_c$

$$\begin{cases} y(t) = \text{Re} \{ \tilde{y}(t) e^{j2\pi f_c t} \} = y_I(t) \cos(2\pi f_c t) - y_Q(t) \sin(2\pi f_c t) \\ \tilde{y}(t) = y_I(t) + jy_Q(t) \end{cases}$$



Bandpass System

- Question: Is the following system valid?



- The advantage of the above equivalent system is that there is no need to deal with the *carrier frequency* in the system analysis.
- The answer to the question is YES (**with some modification**)! It will be substantiated in the sequel.

It suffices to show that $\tilde{Y}(f) = \tilde{X}(f)\tilde{H}(f)$.

$$\text{Observe that } \begin{cases} Y_+(f) = 2u(f)Y(f) \\ X_+(f) = 2u(f)X(f) \\ H_+(f) = 2u(f)H(f) \end{cases} \text{ and } \begin{cases} \tilde{Y}(f) = Y_+(f + f_c) \\ \tilde{X}(f) = X_+(f + f_c) \\ \tilde{H}(f) = H_+(f + f_c) \end{cases}$$

Consequently,

$$\begin{aligned} \tilde{X}(f)\tilde{H}(f) &= X_+(f + f_c)H_+(f + f_c) \\ &= (2u(f + f_c)X(f + f_c))(2u(f + f_c)H(f + f_c)) \\ &= 4u(f + f_c)X(f + f_c)H(f + f_c) \\ &= 4u(f + f_c)Y(f + f_c) \\ &= 2Y_+(f + f_c) \\ &= 2\tilde{Y}(f) \longrightarrow \end{aligned}$$

There is an additional multiplicative constant **2** at the output!

Bandpass System

□ Conclusion:

$$\tilde{x}(t) \rightarrow \boxed{\tilde{h}(\tau)} \rightarrow \tilde{y}(t) = \frac{1}{2} \int_{-\infty}^{\infty} \tilde{h}(\tau) \tilde{x}(t - \tau) d\tau$$

Bandpass System

□ Final note on bandpass system

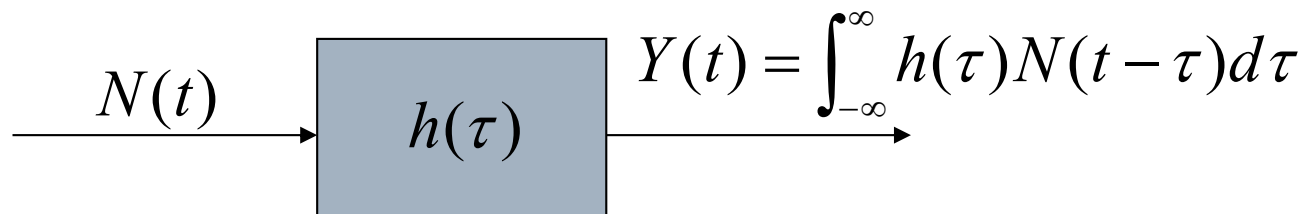
- Some books define $H_+(f) = u(f)H(f)$ for a **filter**, instead of $H_+(f) = 2u(f)H(f)$ (as for a **signal**).
- As a result of this definition (i.e., $H_+(f) = u(f)H(f)$),

$$h(\tau) = 2 \operatorname{Re} \left\{ \tilde{h}(\tau) e^{j2\pi f_c \tau} \right\} \text{ and } \tilde{y}(t) = \int_{-\infty}^{\infty} \tilde{h}(\tau) \tilde{x}(t - \tau) d\tau$$

- It is justifiable to remove 2 in $H_+(f) = u(f)H(f)$, because a **filter** is used to **filter out** the signal; hence, it is not necessary to *make the total area constant*.

Representation of Narrowband Noise using In-Phase and Quadrature Components

- The bandpass system representation discussed previously is based on *deterministic signals*.
- How about a random process? Can we have a low-pass isomorphism system to a bandpass random process.
 - Take the noise process $N(t)$ as an example.



Representation of Narrowband Noise using In-Phase and Quadrature Components

□ A WSS *real-valued zero-mean* noise process $N(t)$ is a bandpass process if its PSD $S_N(f) \neq 0$ only for $|f - f_c| < B$ and $|f + f_c| < B$, and also $B < f_c$.

■ Similar to the analysis for deterministic signals, let

$$\begin{cases} N(t) = N_I(t) \cos(2\pi f_c t) - N_Q(t) \sin(2\pi f_c t) \\ \tilde{N}(t) = N_I(t) + jN_Q(t) \end{cases}$$

for some joint zero-mean WSS of $N_I(t)$ and $N_Q(t)$.

■ Notably, the joint WSS of $N_I(t)$ and $N_Q(t)$ immediately imply WSS of $\tilde{N}(t)$.

PSD of $N_I(t)$ and $N_Q(t)$

- First, we note that joint WSS of $N_I(t)$ and $N_Q(t)$ and the WSS of $N(t)$ imply:

$$\begin{cases} R_{N_I}(\tau) = R_{N_Q}(\tau) \\ R_{N_I, N_Q}(\tau) = -R_{N_Q, N_I}(\tau) \end{cases} \quad (\text{See the proof in the sequel.})$$

$$\begin{aligned}
R_N(\tau) &= E[N(t + \tau)N(t)] \\
&= E[(N_I(t + \tau) \cos(2\pi f_c(t + \tau)) - N_Q(t + \tau) \sin(2\pi f_c(t + \tau))) \\
&\quad \times (N_I(t) \cos(2\pi f_c t) - N_Q(t) \sin(2\pi f_c t))] \\
&= R_{N_I}(\tau) \cos(2\pi f_c(t + \tau)) \cos(2\pi f_c t) \\
&\quad + R_{N_Q}(\tau) \sin(2\pi f_c(t + \tau)) \sin(2\pi f_c t) \\
&\quad - R_{N_I, N_Q}(\tau) \cos(2\pi f_c(t + \tau)) \sin(2\pi f_c t) \\
&\quad - R_{N_Q, N_I}(\tau) \sin(2\pi f_c(t + \tau)) \cos(2\pi f_c t) \\
&= R_{N_I}(\tau) \frac{\cos(2\pi f_c \tau) + \cos(2\pi f_c(2t + \tau))}{2} \\
&\quad + R_{N_Q}(\tau) \frac{\cos(2\pi f_c \tau) - \cos(2\pi f_c(2t + \tau))}{2} \\
&\quad - R_{N_I, N_Q}(\tau) \frac{\sin(2\pi f_c(2t + \tau)) - \sin(2\pi f_c \tau)}{2} \\
&\quad - R_{N_Q, N_I}(\tau) \frac{\sin(2\pi f_c(2t + \tau)) + \sin(2\pi f_c \tau)}{2}
\end{aligned}$$

(Continue from the previous slide.)

These two terms must equal zero, since $R_N(\tau)$ is not a function of t .

$$\begin{aligned} R_N(\tau) = & \frac{1}{2} [R_{N_I}(\tau) + R_{N_Q}(\tau)] \cos(2\pi f_c \tau) \\ & + \frac{1}{2} [R_{N_I, N_Q}(\tau) - R_{N_Q, N_I}(\tau)] \sin(2\pi f_c \tau) \\ & + \frac{1}{2} [R_{N_I}(\tau) - R_{N_Q}(\tau)] \cos(2\pi f_c (2t + \tau)) \\ & - \frac{1}{2} [R_{N_I, N_Q}(\tau) + R_{N_Q, N_I}(\tau)] \sin(2\pi f_c (2t + \tau)) \end{aligned}$$

$$\Rightarrow \begin{cases} R_{N_I}(\tau) = R_{N_Q}(\tau) \\ R_{N_I, N_Q}(\tau) = -R_{N_Q, N_I}(\tau) \end{cases} \quad \text{(Property 1)}$$

$$\Rightarrow R_N(\tau) = R_{N_I}(\tau) \cos(2\pi f_c \tau) - R_{N_Q, N_I}(\tau) \sin(2\pi f_c \tau) \quad \text{(Property 2)}$$

PSD of $N_I(t)$ and $N_Q(t)$

■ Some other properties

$$\begin{aligned} R_{\tilde{N}}(\tau) &= E[\tilde{N}(t + \tau)\tilde{N}^*(t)] \\ &= E[(N_I(t + \tau) + jN_Q(t + \tau)) \times (N_I(t) - jN_Q(t))] \\ &= R_{N_I}(\tau) + R_{N_Q}(\tau) + j[R_{N_Q, N_I}(\tau) - R_{N_I, N_Q}(\tau)] \\ &= 2R_{N_I}(\tau) + j2R_{N_Q, N_I}(\tau) \quad \textbf{(Property 3)} \end{aligned}$$

PSD of $N_I(t)$ and $N_Q(t)$

Properties 2 and 3 jointly imply

$$R_N(\tau) = \frac{1}{2} \operatorname{Re}\{R_{\tilde{N}}(\tau) \exp(j2\pi f_c \tau)\} \quad \text{(Property 4)}$$

□ As the inconsistency encountered in Slide 3-24,

■ some books define

$$\begin{cases} R_{\tilde{X}}(\tau) = \frac{1}{2} E[\tilde{X}(t+\tau)\tilde{X}^*(t)] & \text{for complex } \tilde{X}(t); \\ R_X(\tau) = E[X(t+\tau)X(t)] & \text{for real } X(t) \end{cases}$$

■ As a result of the two “inconsistent” definitions, a “simpler” relation is obtained: $R_N(\tau) = \operatorname{Re}\{R_{\tilde{N}}(\tau) \exp(j2\pi f_c \tau)\}$

■ For consistency, we let $R_{\tilde{X}}(\tau) = E[\tilde{X}(t+\tau)\tilde{X}^*(t)]$ for complex $\tilde{X}(t)$

Summary of Spectrum Properties

1. $R_{N_I}(\tau) = R_{N_Q}(\tau)$ and $R_{N_I, N_Q}(\tau) = -R_{N_Q, N_I}(\tau)$

2. $R_N(\tau) = R_{N_I}(\tau) \cos(2\pi f_c \tau) - R_{N_Q, N_I}(\tau) \sin(2\pi f_c \tau)$

3. $R_{\tilde{N}}(\tau) = 2 \cdot R_{N_I}(\tau) + j2 \cdot R_{N_Q, N_I}(\tau) \Rightarrow R_N(0) = R_{N_I}(0) = R_{N_Q}(0)$

4. $R_N(\tau) = \frac{1}{2} \cdot \text{Re}\{R_{\tilde{N}}(\tau) \exp(j2\pi f_c \tau)\}$

5. $S_{\tilde{N}}(f)$ is real-valued. \longrightarrow By $R_{\tilde{N}}(\tau) = R_{\tilde{N}}^*(-\tau)$.

6. $S_{N_I}(f) = S_{N_Q}(f)$ and $S_{N_I, N_Q}(f) = -S_{N_Q, N_I}(f)$ [From 1.]

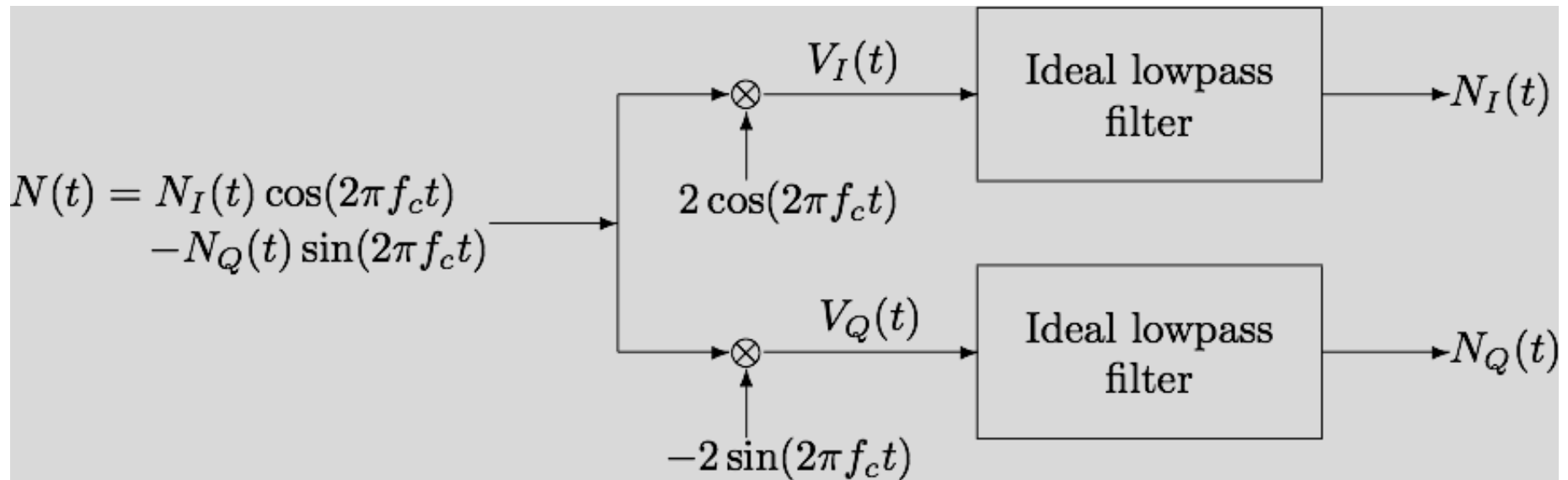
7. $S_N(f) = \frac{1}{4} (S_{\tilde{N}}(f - f_c) + S_{\tilde{N}}(-f - f_c))$ [From 4.
See the next slide.]

$$\begin{aligned}
S_N(f) &= \int_{-\infty}^{\infty} R_N(\tau) e^{-j2\pi f\tau} d\tau \\
&= \int_{-\infty}^{\infty} \frac{1}{2} \operatorname{Re}\{R_{\tilde{N}}(\tau) e^{j2\pi f_c\tau}\} e^{-j2\pi f\tau} d\tau \\
&= \int_{-\infty}^{\infty} \frac{1}{4} (R_{\tilde{N}}(\tau) e^{j2\pi f_c\tau} + (R_{\tilde{N}}(\tau) e^{j2\pi f_c\tau})^*) e^{-j2\pi f\tau} d\tau \\
&= \int_{-\infty}^{\infty} \frac{1}{4} (R_{\tilde{N}}(\tau) e^{j2\pi f_c\tau} + R_{\tilde{N}}^*(\tau) e^{-j2\pi f_c\tau}) e^{-j2\pi f\tau} d\tau \\
&= \frac{1}{4} \int_{-\infty}^{\infty} R_{\tilde{N}}(\tau) e^{-j2\pi(f-f_c)\tau} d\tau + \frac{1}{4} \left(\int_{-\infty}^{\infty} R_{\tilde{N}}(\tau) e^{-j2\pi(-f-f_c)\tau} d\tau \right)^* \\
&= \frac{1}{4} (S_{\tilde{N}}(f-f_c) + S_{\tilde{N}}^*(-f-f_c)) \\
&= \frac{1}{4} (S_{\tilde{N}}(f-f_c) + S_{\tilde{N}}(-f-f_c))
\end{aligned}$$

8. $N_I(t)$ and $N_Q(t)$ are orthogonal.

$$\begin{cases} R_{N_I, N_Q}(\tau) = -R_{N_Q, N_I}(\tau) \\ R_{N_I, N_Q}(-\tau) = E[N_I(t)N_Q(t+\tau)] = R_{N_Q, N_I}(\tau) \end{cases}$$
$$\Rightarrow R_{N_I, N_Q}(\tau) = -R_{N_I, N_Q}(-\tau)$$
$$\Rightarrow R_{N_I, N_Q}(0) = -R_{N_I, N_Q}(0)$$
$$\Rightarrow R_{N_I, N_Q}(0) = E[N_I(t)N_Q(t)] = 0.$$

$$9. S_{N_I}(f) = S_{N_Q}(f) = \begin{cases} S_N(f - f_c) + S_N(f + f_c), & |f| < B \\ 0, & \text{otherwise} \end{cases}$$



$$\begin{aligned} R_{V_I}(t, u) &= E[V_I(t)V_I(u)] \\ &= 4E[N(t) \cos(2\pi f_c t) N(u) \cos(2\pi f_c u)] \\ &= 4R_N(t, u) \cos(2\pi f_c t) \cos(2\pi f_c u) \end{aligned}$$

Notably, $V_I(t)$ is not WSS.

$$\begin{aligned}
\bar{R}_{V_I}(\tau) &= \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T R_{V_I}(t + \tau, \tau) dt \\
&= \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T 4R_N(\tau) \cos(2\pi f_c(t + \tau)) \cos(2\pi f_c t) dt \\
&= R_N(\tau) \lim_{T \rightarrow \infty} \frac{2}{T} \int_{-T}^T [\cos(2\pi f_c(2t + \tau)) + \cos(2\pi f_c \tau)] dt \\
&= R_N(\tau) \lim_{T \rightarrow \infty} \frac{2}{T} \int_{-T}^T \cos(2\pi f_c(2t + \tau)) dt + 2R_N(\tau) \cos(2\pi f_c \tau) \\
&= 2R_N(\tau) \cos(2\pi f_c \tau)
\end{aligned}$$

$$\bar{S}_{V_I}(f) = S_N(f - f_c) + S_N(f + f_c)$$

$$\bar{S}_{N_I}(f) = |H(f)|^2 \bar{S}_{V_I}(f), \text{ where } |H(f)|^2 = \begin{cases} 1, & |f| \leq B \\ 0, & f > B \end{cases}$$

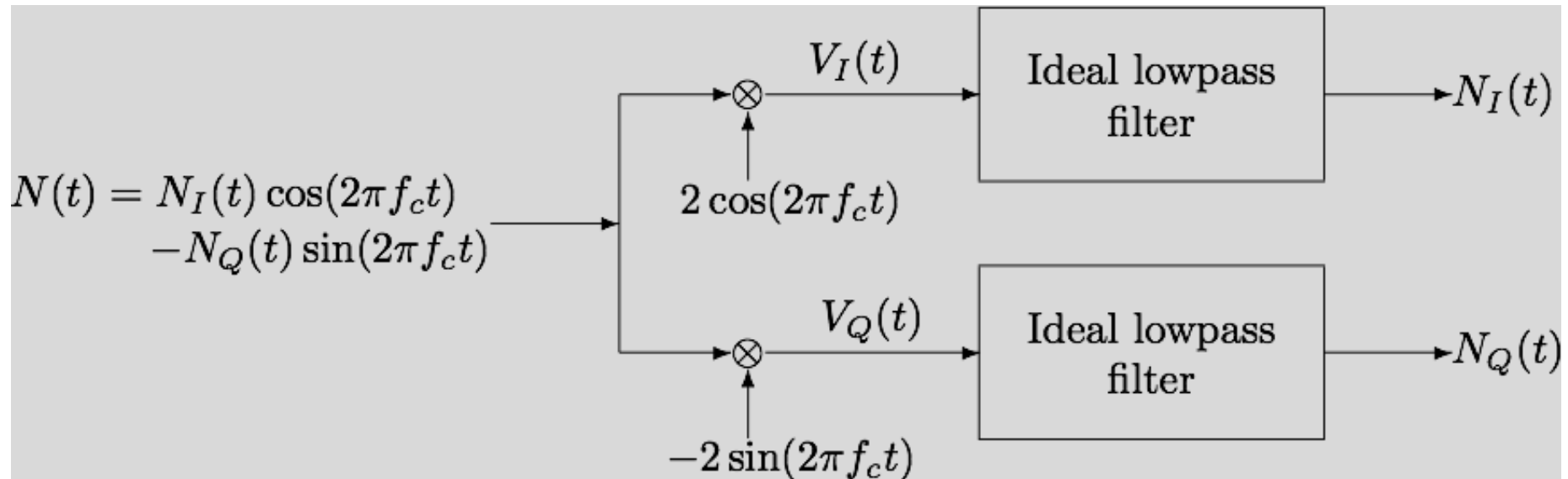
$$\Rightarrow S_{N_I}(f) = \bar{S}_{N_I}(f) = [S_N(f - f_c) + S_N(f + f_c)] |H(f)|^2 \\ = \begin{cases} S_N(f - f_c) + S_N(f + f_c), & |f| < B \\ 0, & \text{otherwise} \end{cases}$$

Similarly,

$$S_{N_Q}(f) = \begin{cases} S_N(f - f_c) + S_N(f + f_c), & |f| < B \\ 0, & \text{otherwise} \end{cases}$$

This result (namely, $S_{N_I}(f) = S_{N_Q}(f)$) coincides with Property 1, for which $R_{N_I}(\tau) = R_{N_Q}(\tau)$.

$$10. S_{N_I, N_Q}(f) = \begin{cases} j[S_N(f + f_c) - S_N(f - f_c)], & |f| < B \\ 0, & \text{otherwise} \end{cases}$$



$$\begin{aligned} R_{V_I, V_Q}(t, u) &= E[V_I(t)V_Q(u)] \\ &= -4E[N(t) \cos(2\pi f_c t) N(u) \sin(2\pi f_c u)] \\ &= -4R_N(t, u) \cos(2\pi f_c t) \sin(2\pi f_c u) \end{aligned}$$

$$R_{V_I, V_Q}(t + \tau, t) = -4R_N(\tau) \cos(2\pi f_c (t + \tau)) \sin(2\pi f_c t)$$

$$\begin{aligned}
\bar{R}_{V_I, V_Q}(\tau) &= \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T R_{V_I, V_Q}(t + \tau, t) dt \\
&= -R_N(\tau) \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T}^T [\sin(2\pi f_c(2t + \tau)) - \sin(2\pi f_c \tau)] dt \\
&= 2R_N(\tau) \sin(2\pi f_c \tau)
\end{aligned}$$

$$\bar{S}_{V_I, V_Q}(f) = j[S_N(f + f_c) - S_N(f - f_c)]$$

$$\begin{aligned}
R_{N_I, N_Q}(t, u) &= E[N_I(t)N_Q(u)] \\
&= E\left[\int_{-\infty}^{\infty} h_I(\tau_1)V_I(t - \tau_1)d\tau_1 \cdot \int_{-\infty}^{\infty} h_Q(\tau_2)V_Q(u - \tau_2)d\tau_2\right] \\
&= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} h_I(\tau_1)h_Q(\tau_2)E[V_I(t - \tau_1)V_Q(u - \tau_2)]d\tau_1d\tau_2 \\
&= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} h_I(\tau_1)h_Q(\tau_2)R_{V_I, V_Q}(t - \tau_1, u - \tau_2)d\tau_1d\tau_2
\end{aligned}$$

$$\begin{aligned}
& \bar{R}_{N_I, N_Q}(\tau) \\
&= \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T R_{N_I, N_Q}(t + \tau, t) dt \\
&= \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} h_I(\tau_1) h_Q(\tau_2) R_{V_I, V_Q}(t + \tau - \tau_1, t - \tau_2) d\tau_1 d\tau_2 dt \\
&= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} h_I(\tau_1) h_Q(\tau_2) \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T R_{V_I, V_Q}(t + \tau - \tau_1, t - \tau_2) dt d\tau_1 d\tau_2 \\
&= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} h_I(\tau_1) h_Q(\tau_2) \bar{R}_{V_I, V_Q}(\tau - \tau_1 + \tau_2) d\tau_1 d\tau_2
\end{aligned}$$

$$\begin{aligned}\bar{S}_{N_I, N_Q}(f) &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} h_I(\tau_1) h_Q(\tau_2) \bar{R}_{V_I, V_Q}(\tau_2 + \tau - \tau_1) e^{-j2\pi f \tau} d\tau d\tau_1 d\tau_2 \\ &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} h_I(\tau_1) h_Q(\tau_2) \bar{R}_{V_I, V_Q}(u) e^{-j2\pi f(u - \tau_2 + \tau_1)} du d\tau_1 d\tau_2,\end{aligned}$$

(Let $u = \tau_2 + \tau - \tau_1$.)

$$= H_I(f) H_Q(-f) \bar{S}_{V_I, V_Q}(f)$$

Here, $H_Q(-f) = H_Q^*(f)$.

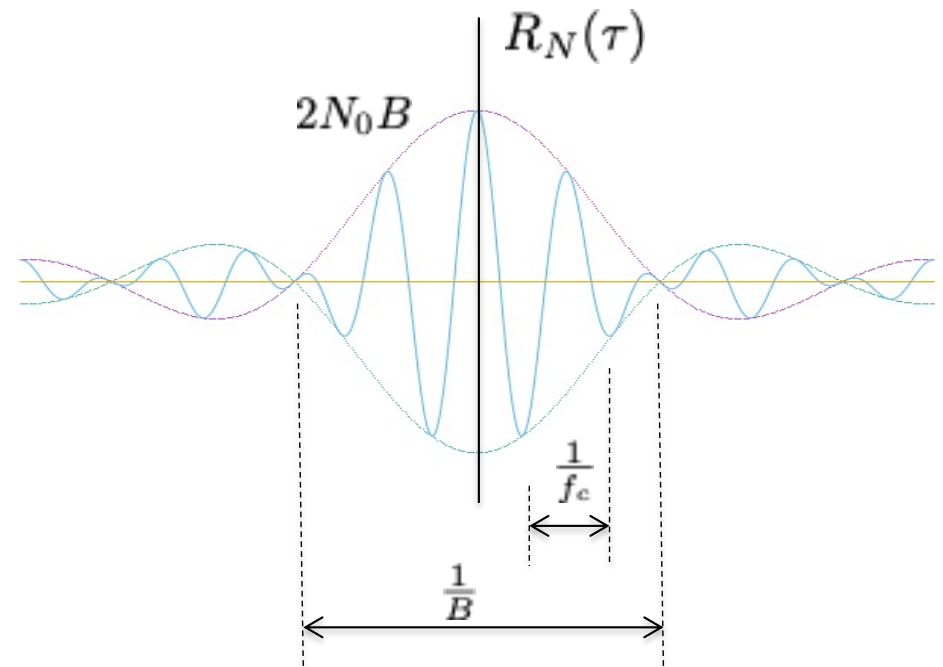
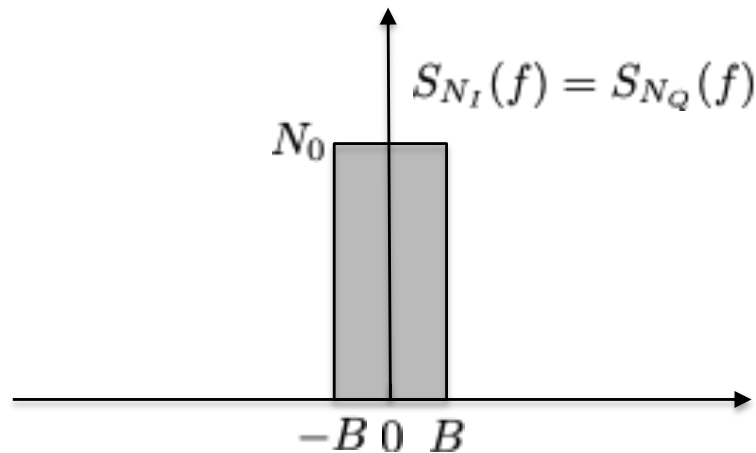
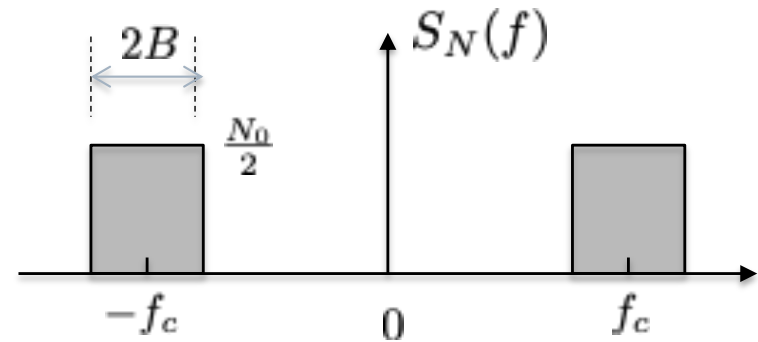
Take $H_I(f) = H_Q(f) = H(f)$.

Then $H_I(f) H_Q(-f) = H(f) H(-f) = H(f) H^*(f) = |H(f)|^2$.

$$\begin{aligned}S_{N_I, N_Q}(f) &= \bar{S}_{N_I, N_Q}(f) \\ &= j[S_N(f + f_c) - S_N(f - f_c)] |H(f)|^2 \\ &= \begin{cases} j[S_N(f + f_c) - S_N(f - f_c)], & |f| < B \\ 0, & \text{otherwise} \end{cases}\end{aligned}$$

Ideal Bandpass Filtered White Noise Revisited

$$\begin{aligned}
 R_N(\tau) &= \int_{-f_c-B}^{-f_c+B} \frac{N_0}{2} e^{j2\pi f\tau} df \\
 &\quad + \int_{f_c-B}^{f_c+B} \frac{N_0}{2} e^{j2\pi f\tau} df \\
 &= 2BN_0 \text{sinc}(2B\tau) \cos(2\pi f_c\tau) \\
 R_{N_I}(\tau) &= 2BN_0 \text{sinc}(2B\tau)
 \end{aligned}$$



Representation of Narrowband Noise using Envelope and Phase Components

- Now we turn to *envelope* $R(t)$ and *phase* $\Psi(t)$ **components** of a random process of the form

$$\begin{aligned} N(t) &= N_I(t) \cos(2\pi f_c t) - N_Q(t) \sin(2\pi f_c t) \\ &= R(t) \cos[2\pi f_c t + \Psi(t)] \end{aligned}$$

where $R(t) = \sqrt{N_I^2(t) + N_Q^2(t)}$ and $\Psi(t) = \tan^{-1}[N_Q(t)/N_I(t)]$.

Pdf of $R(t)$ and $\Psi(t)$

- Assume that $N(t)$ is a white Gaussian process with two-sided PSD $\sigma^2 = N_0/2$.
- For convenience, let N_I and N_Q be snapshot samples of $N_I(t)$ and $N_Q(t)$.
- Then

$$f_{N_I, N_Q}(n_I, n_Q) = \frac{1}{2\pi\sigma^2} \exp\left(-\frac{n_I^2 + n_Q^2}{2\sigma^2}\right)$$

Pdf of $R(t)$ and $\Psi(t)$

□ By $n_I = r \cos(\psi)$ and $n_Q = r \sin(\psi)$,

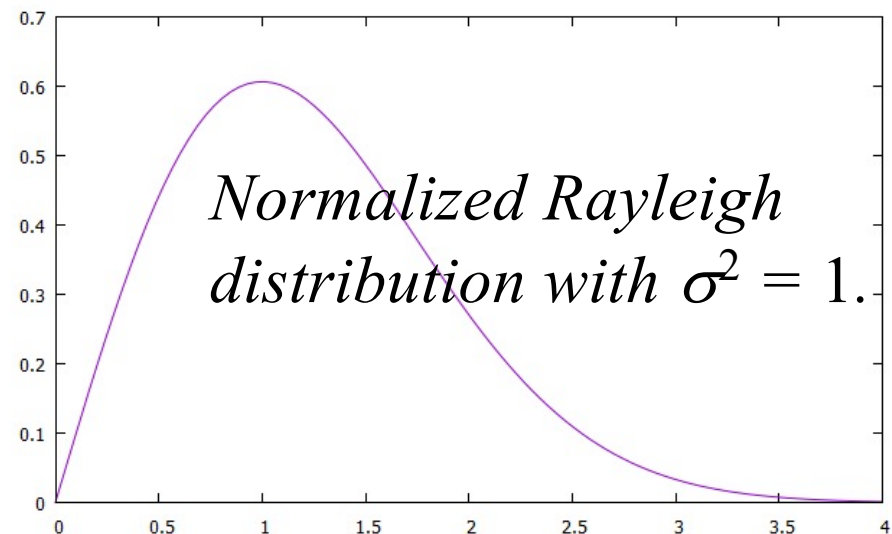
$$\begin{aligned} \int_{A(n_I, n_Q)} \frac{1}{2\pi\sigma^2} \exp\left(-\frac{n_I^2 + n_Q^2}{2\sigma^2}\right) dn_I dn_Q &= \int_{A(r, \psi)} \frac{1}{2\pi\sigma^2} \exp\left(-\frac{r^2}{2\sigma^2}\right) \begin{vmatrix} \frac{dn_I}{dr} & \frac{dn_Q}{dr} \\ \frac{dn_I}{d\psi} & \frac{dn_Q}{d\psi} \end{vmatrix} dr d\psi \\ &= \int_{A(r, \psi)} \frac{1}{2\pi\sigma^2} \exp\left(-\frac{r^2}{2\sigma^2}\right) r dr d\psi \end{aligned}$$

$$\text{So } f_{R, \Psi}(r, \psi) = \frac{r}{2\pi\sigma^2} \exp\left(-\frac{r^2}{2\sigma^2}\right) = \frac{1}{2\pi} \times \frac{r}{\sigma^2} \exp\left(-\frac{r^2}{2\sigma^2}\right).$$

Pdf of $R(t)$ and $\Psi(t)$

□ R and Ψ are therefore independent.

$$\left\{ \begin{array}{l} f_R(r) = \frac{r}{\sigma^2} \exp\left(-\frac{r^2}{2\sigma^2}\right) \text{ for } r \geq 0. \\ f_\Psi(\psi) = \frac{1}{2\pi} \text{ for } 0 \leq \psi < 2\pi. \end{array} \right. \quad \text{Rayleigh distribution.}$$



Sine Wave + Gaussian Noise

□ Now suppose the Gaussian white noise is added to a sinusoid of amplitude A .

□ Then

$$\begin{aligned}x(t) &= A \cos(2\pi f_c t) + n(t) \\ &= A \cos(2\pi f_c t) + n_I(t) \cos(2\pi f_c t) - n_Q(t) \sin(2\pi f_c t) \\ &= x_I(t) \cos(2\pi f_c t) - x_Q(t) \sin(2\pi f_c t)\end{aligned}$$

■ Uncorrelation for Gaussian $n_I(t)$ and $n_Q(t)$ implies their independence.

Sine Wave + Gaussian Noise

□ This gives the pdf of $x_I(t)$ and $x_Q(t)$ as:

$$f_{x_I, x_Q}(x_I, x_Q) = \frac{1}{2\pi\sigma^2} \exp\left[-\frac{(x_I - A)^2 + x_Q^2}{2\sigma^2}\right]$$

□ By $x_I = r \cos(\psi)$ and $x_Q = r \sin(\psi)$,

$$f_{R, \Psi}(r, \psi) = \frac{1}{2\pi\sigma^2} \exp\left[-\frac{(r \cos(\psi) - A)^2 + r^2 \sin^2(\psi)}{2\sigma^2}\right] \begin{vmatrix} \frac{dx_I}{dr} & \frac{dx_Q}{dr} \\ \frac{dx_I}{d\psi} & \frac{dx_Q}{d\psi} \end{vmatrix}$$

$$= \frac{r}{2\pi\sigma^2} \exp\left(-\frac{r^2 + A^2 - 2Ar \cos(\psi)}{2\sigma^2}\right)$$

Sine Wave + Gaussian Noise

- Notably, in this case, R and Ψ are no longer independent.
- We are more interested in the marginal distribution of R .

$$\begin{aligned} f_R(r) &= \int_0^{2\pi} f_{R,\Psi}(r,\psi) d\psi \\ &= \int_0^{2\pi} \frac{r}{2\pi\sigma^2} \exp\left(-\frac{r^2 + A^2 - 2Ar \cos(\psi)}{2\sigma^2}\right) d\psi \end{aligned}$$

Sine Wave + Gaussian Noise

$$\begin{aligned} f_R(r) &= \frac{r}{2\pi\sigma^2} \exp\left(-\frac{r^2 + A^2}{2\sigma^2}\right) \int_0^{2\pi} \exp\left(\frac{2Ar \cos(\psi)}{2\sigma^2}\right) d\psi \\ &= \frac{r}{\sigma^2} \exp\left(-\frac{r^2 + A^2}{2\sigma^2}\right) I_0\left(\frac{Ar}{\sigma^2}\right), \end{aligned}$$

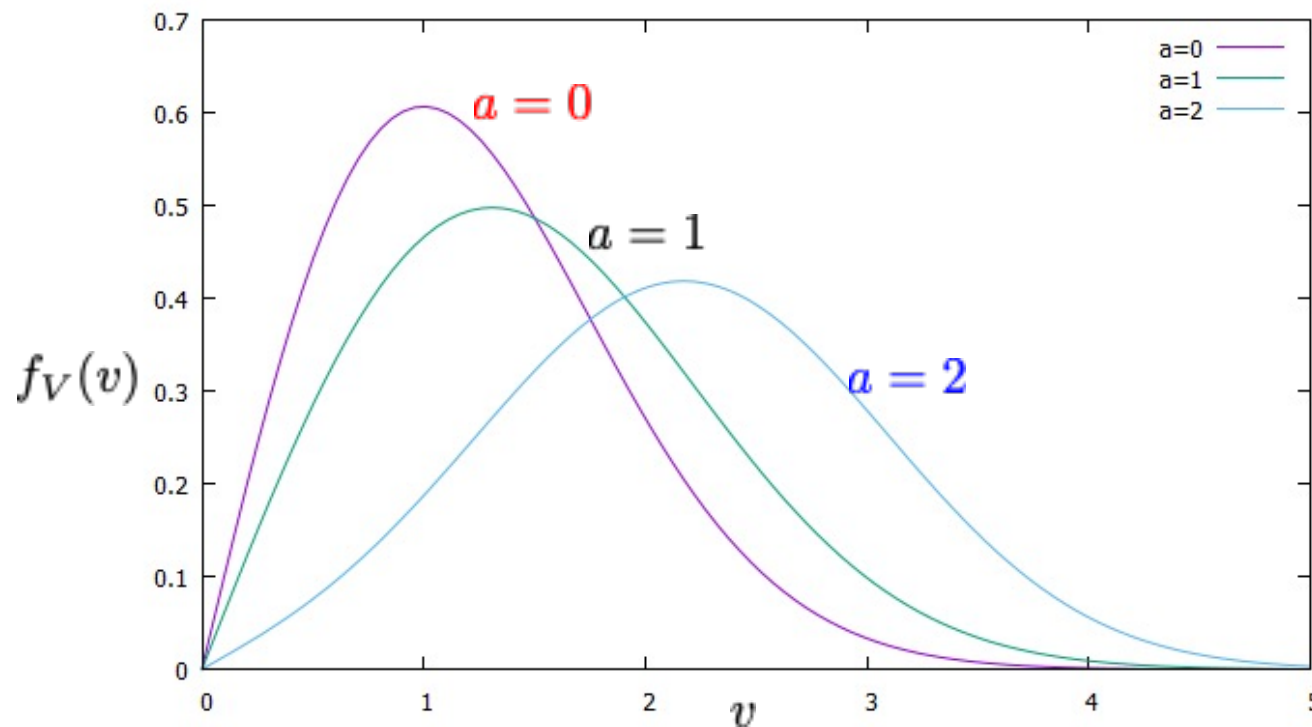
where $I_0(x) = \frac{1}{2\pi} \int_0^{2\pi} \exp(x \cos(\psi)) d\psi$ is the modified Bessel function of the first kind of zero order.

This distribution is named the *Rician distribution*.

Normalized Rician distribution

Let $v = \frac{r}{\sigma}$ and $a = \frac{A}{\sigma}$.

$$f_V(v) = v \cdot \exp\left(-\frac{v^2 + a^2}{2}\right) I_0(av),$$



Bessel Functions

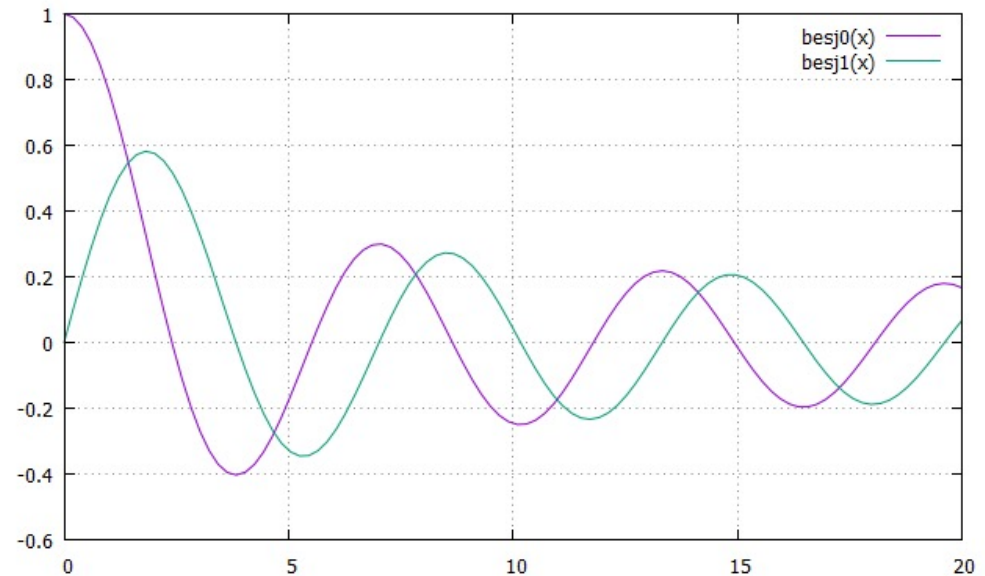
- Bessel's equation of order n

$$x^2 \frac{d^2 y}{dx^2} + x \frac{dy}{dx} + (x^2 - n^2)y = 0$$

- Its solution $J_n(x)$ is the *Bessel function of the first kind of order n* .

$$J_n(x) = \frac{1}{\pi} \int_0^\pi \cos(x \sin(\theta) - n\theta) d\theta$$

$$= \frac{1}{2\pi} \int_{-\pi}^\pi \exp(jx \sin \theta - jn\theta) d\theta = \sum_{m=0}^{\infty} \frac{(-1)^m (x/2)^{n+2m}}{m!(n+m)!}$$



Properties of the Bessel Function

1. $J_n(x) = (-1)^n J_{-n}(x) = (-1)^n J_n(-x)$

2. $J_{n-1}(x) + J_{n+1}(x) = \frac{2n}{x} J_n(x)$ 3. When x small, $J_n(x) \approx \frac{x^n}{2^n n!}$.

4. When x large, $J_n(x) \approx \sqrt{\frac{2}{\pi x}} \cos\left(x - \frac{\pi}{4} - \frac{n\pi}{2}\right)$

5. $\lim_{n \rightarrow \infty} J_n(x) = 0$. 6. $\sum_{n=-\infty}^{\infty} J_n(x) \exp(jn\phi) = \exp(jx \sin(\phi))$

7. $\sum_{n=-\infty}^{\infty} J_n^2(x) = 1$.

Modified Bessel Function

- Modified Bessel's equation of order n

$$x^2 \frac{d^2 y}{dx^2} + x \frac{dy}{dx} + (j^2 x^2 - n^2) y = 0 \quad (\text{i.e., } x^2 \frac{d^2 y}{dx^2} + x \frac{dy}{dx} - (x^2 + n^2) y = 0)$$

- Its solution $I_n(x)$ is the *Modified Bessel function of the first kind of order n* .

$$\begin{aligned} I_n(x) &= j^{-n} J_n(jx) = \frac{1}{2\pi} \int_{-\pi}^{\pi} \exp(x \cos(\theta)) \cos(n\theta) d\theta \\ &= \sum_{m=0}^{\infty} \frac{(x/2)^{n+2m}}{m!(n+m)!} \end{aligned}$$

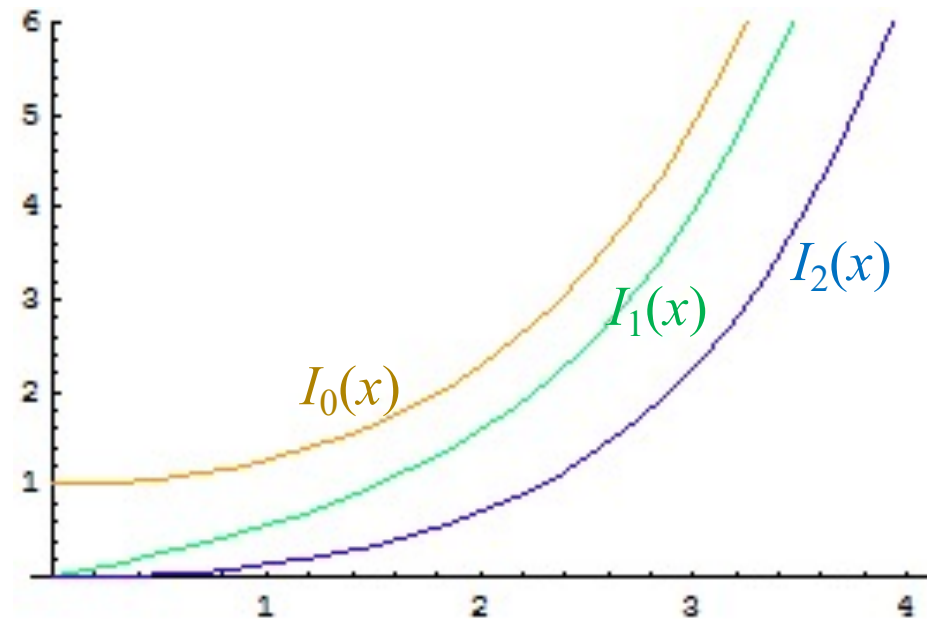
- The modified Bessel function is monotonically increasing in x for all n .

Properties of Modified Bessel Function

$$3'. \lim_{x \downarrow 0} I_n(x) = \begin{cases} 1, & n = 0 \\ 0, & n \geq 1 \end{cases}$$

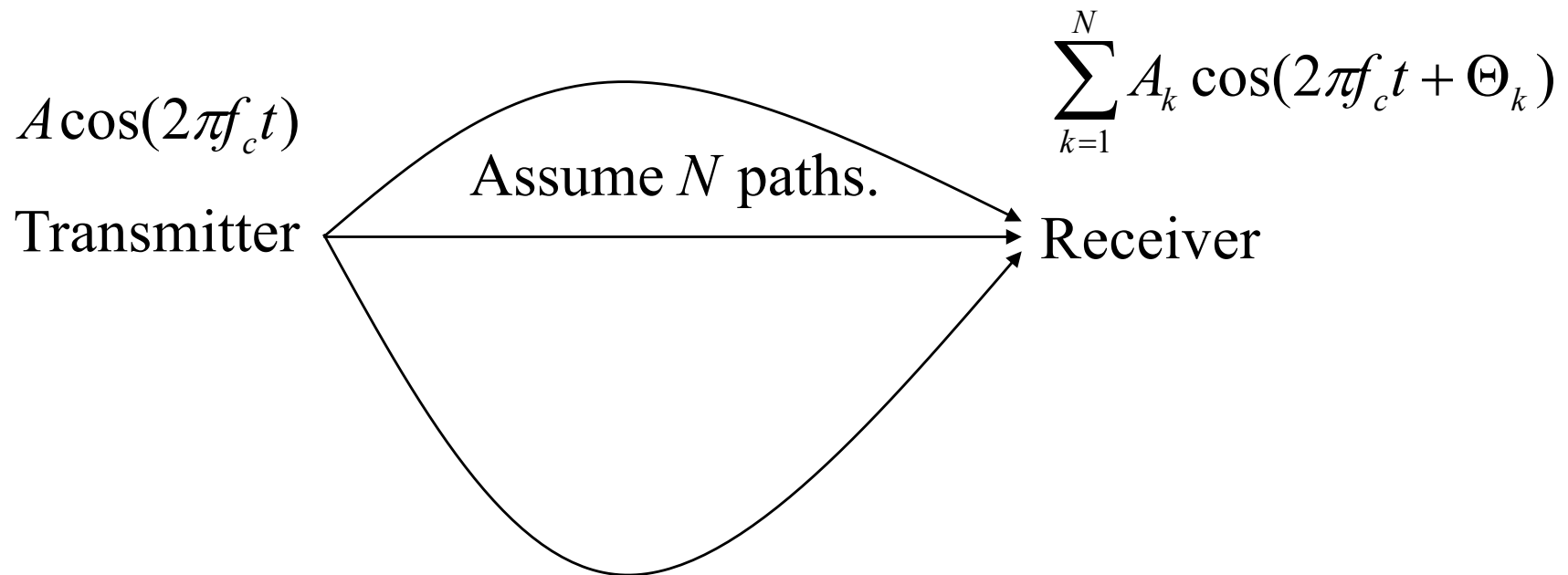
$$4'. \text{When } x \text{ large, } I_n(x) \approx \frac{\exp(x)}{\sqrt{2\pi x}}.$$

$$6'. \sum_{n=-\infty}^{\infty} I_n(x) \exp(jn\phi) = \exp(x \cos(\phi))$$



Flat-Fading Channel

□ Model of a multi-path channel



Flat-Fading Channel

$$Y(t) = \sum_{k=1}^N A_k \cos(2\pi f_c t + \Theta_k) = Y_I \cos(2\pi f_c t) - Y_Q \sin(2\pi f_c t)$$

where $Y_I = \sum_{k=1}^N A_k \cos(\Theta_k)$ and $Y_Q = \sum_{k=1}^N A_k \sin(\Theta_k)$.

\Rightarrow Input $\tilde{X}(t) = A$ induces output $\tilde{Y}(t) = Y_I + jY_Q$,
which is independent of t .

Assume $\{(A_k, \Theta_k)\}$ i.i.d., and A_k uniform over $[-1, +1)$
and Θ_k uniform over $[0, 2\pi)$.

Flat-Fading Channel

□ By Central Limit Theorem,

$$\frac{Y_I}{\sqrt{N/6}} = \frac{A_1 \cos(\Theta_1) + \dots + A_N \cos(\Theta_N)}{\sqrt{N/6}} \rightarrow \text{Normal}(0,1)$$

So Y_I is approximately Gaussian distributed with mean 0 and variance $(N/6)$.

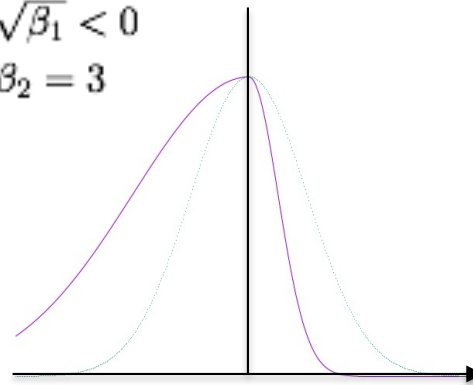
For any Gaussian random variable G , we have

$$\sqrt{\beta_1} = \frac{E[(G - \mu)^3]}{E^{3/2}[(G - \mu)^2]} = 0 \text{ and } \beta_2 = \frac{E[(G - \mu)^4]}{E^2[(G - \mu)^2]} = 3.$$

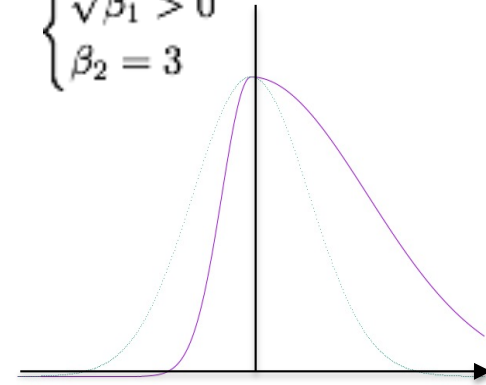
Flat-Fading Channel

$\sqrt{\beta_1}$ skewness
 β_2 kurtosis

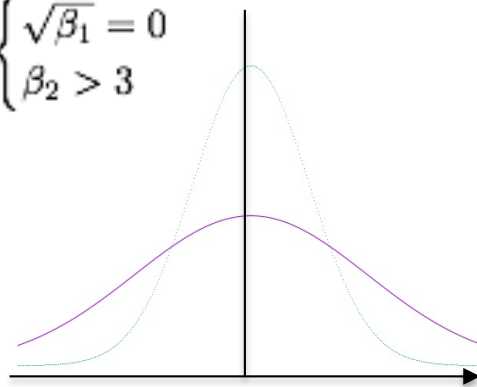
$$\begin{cases} \sqrt{\beta_1} < 0 \\ \beta_2 = 3 \end{cases}$$



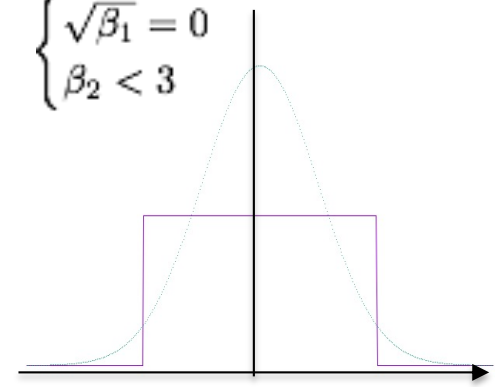
$$\begin{cases} \sqrt{\beta_1} > 0 \\ \beta_2 = 3 \end{cases}$$



$$\begin{cases} \sqrt{\beta_1} = 0 \\ \beta_2 > 3 \end{cases}$$



$$\begin{cases} \sqrt{\beta_1} = 0 \\ \beta_2 < 3 \end{cases}$$



Flat-Fading Channel

- Normality Test: We can therefore use β_1 and β_2 to examine the degree of resemblance to Gaussian for a random variable.

$$S_N = (U_1 + \dots + U_N) / a_N \text{ for zero - mean i.i.d. } \{U_k\}$$

$$\Rightarrow \tilde{\beta}_2 = \frac{E[S_N^4]}{E^2[S_N^2]} = \frac{E[(U_1 + \dots + U_N)^4]}{E^2[(U_1 + \dots + U_N)^2]} = \frac{NE[U^4] + 3N(N-1)E^2[U^2]}{N^2E^2[U^2]} = 3 + \frac{E[U^4]/E^2[U^2] - 3}{N}$$

$$\Rightarrow \begin{cases} E[A \cos(\Theta)] = E[A \sin(\Theta)] = 0 \\ E[A^2 \cos^2(\Theta)] = E[A^2 \sin^2(\Theta)] = 1/6 \\ E[A^4 \cos^4(\Theta)] = E[A^4 \sin^4(\Theta)] = 3/40 \end{cases}$$

$N = 10$	100	1000	10000
2.97	2.997	2.9997	2.99997

Summary

- Narrowband process
 - Hilbert transform
 - Bandpass system
- Gaussian, Rayleigh and Rician
 - Central Limit Theorem