

Digital Communications

Chapter 9 Digital Communications Through Band-Limited Channels

Po-Ning Chen, Professor

Institute of Communications Engineering
National Chiao-Tung University, Taiwan

9.2 Signal design for band-limited channels

For the baseband waveform

$$s_{\ell}(t) = \sum_{n=-\infty}^{\infty} I_n g(t - nT)$$

- Channel is band-limited to $[-W, W]$.
- Transmitted signals outside $[-W, W]$ will be truncated.

How to design $g(t)$ to yield optimal performance?

¹ Here we use $s_{\ell}(t)$ instead of $v(t)$ as being used in text to clearly indicate that $s_{\ell}(t)$ is the lowpass equivalent signal of $s(t)$.

Recall that

$$s_\ell(t) = \sum_{n=-\infty}^{\infty} I_n g(t - nT)$$

is a cyclostationary random process with i.i.d. discrete random process $\{I_n\}$.

- Autocorrelation function of $s_\ell(t)$ is

$$R_{s_\ell}(t + \tau, t) = \mathbb{E}[s_\ell(t + \tau)s_\ell^*(t)]$$

is periodic with period T .

- The time-average autocorrelation function

$$\begin{aligned}\bar{R}_{s_\ell}(\tau) &= \frac{1}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} R_{s_\ell}(t + \tau, t) dt \\ &= \frac{1}{T} \sum_{n=-\infty}^{\infty} R_I(n) \int_{-\infty}^{\infty} g(t + \tau - nT)g^*(t) dt\end{aligned}$$

$$\bar{R}_{s_\ell}(\tau) = \frac{1}{T} \sum_n R_I(n) \int_{-\infty}^{\infty} g(t + \tau - nT) g^*(t) dt$$

- The time-average power spectral density of $s_\ell(t)$ is

$$\begin{aligned} \bar{S}_{s_\ell}(f) &= \int_{-\infty}^{\infty} \bar{R}_{s_\ell}(\tau) e^{-j2\pi f\tau} d\tau \\ &= \frac{1}{T} \left[\sum_{n=-\infty}^{\infty} R_I(n) e^{-j2\pi fnT} \right] |G(f)|^2 \end{aligned}$$

- Assuming I_n is zero mean and i.i.d., $R_I(n) = \sigma^2 \delta_n$, hence

$$\bar{S}_{s_\ell}(f) = \frac{\sigma^2}{T} |G(f)|^2$$

For static channel with impulse response $c_\ell(t)$, band-limited to $[-W, W]$, i.e.

$$C_\ell(f) = 0 \quad \text{for } |f| > W$$

The received signal is

$$\begin{aligned} r_\ell(t) &= c_\ell(t) * s_\ell(t) + n_\ell(t) \\ &= \int_{-\infty}^{\infty} c_\ell(\tau) \left(\sum_{n=-\infty}^{\infty} I_n g(t - \tau - nT) \right) d\tau + n_\ell(t) \\ &= \sum_{n=-\infty}^{\infty} I_n \int_{-\infty}^{\infty} g(t - nT - \tau) c_\ell(\tau) d\tau + n_\ell(t) \end{aligned}$$

whose time-average power spectral density is

$$\bar{S}_{r_\ell}(f) = \frac{\sigma^2}{T} |G(f)|^2 |C_\ell(f)|^2 + 2N_0 \text{rect}\left(\frac{f}{2W}\right)$$

Note that $n_\ell(t)$ is a band-limited white noise process.

$$r_\ell(t) = \sum_{n=-\infty}^{\infty} I_n h_\ell(t - nT) + n_\ell(t) \text{ with } h_\ell(t) = g(t) \star c_\ell(t)$$

- Assume channel Impulse response $c_\ell(t)$ known to Rx.
- The **match-filtered** received signal is

$$y_\ell(t) = r_\ell(t) \star h_\ell^*(T - t) = \sum_n I_n x_\ell(t - nT) + z_\ell(t)$$

where $x_\ell(t) = h_\ell(t) \star h_\ell^*(T - t)$ and
 $z_\ell(t) = n_\ell(t) \star h_\ell^*(T - t)$.

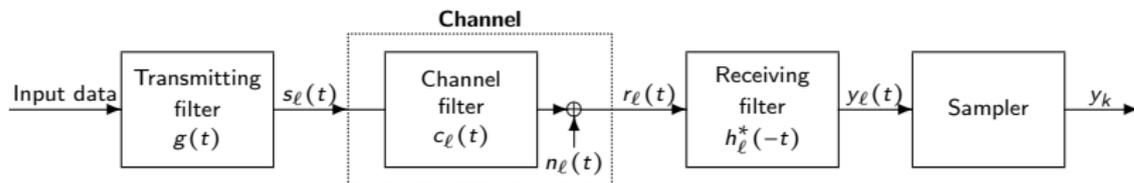
For simplicity, one may use $h_\ell^*(-t)$ instead of $h_\ell^*(T - t)$.

- Sampling at $t = kT$, $k \in \mathbb{Z}$, we get

$$y_k = y_\ell(kT) = \sum_{n=-\infty}^{\infty} I_n x_\ell(kT - nT) + z_\ell(kT) = \sum_n I_n x_{k-n} + z_k$$

where $x_{k-n} = x_\ell(kT - nT)$.

Quick summary



- Transmitted signal $s_\ell(t) = \sum_{n=-\infty}^{\infty} I_n g(t - nT)$
- Received signal $r_\ell(t) = \sum_{n=-\infty}^{\infty} I_n h_\ell(t - nT) + n_\ell(t)$ with $h_\ell(t) = g(t) * c_\ell(t)$.
- Matched filter output $y_\ell(t) = \sum_{n=-\infty}^{\infty} I_n x_\ell(t - nT) + z_\ell(t)$ with $x_\ell(t) = h_\ell(t) * h_\ell^*(-t)$ or equivalently

$$X_\ell(f) = |H_\ell(f)|^2 = |G(f)|^2 |C_\ell(f)|^2.$$

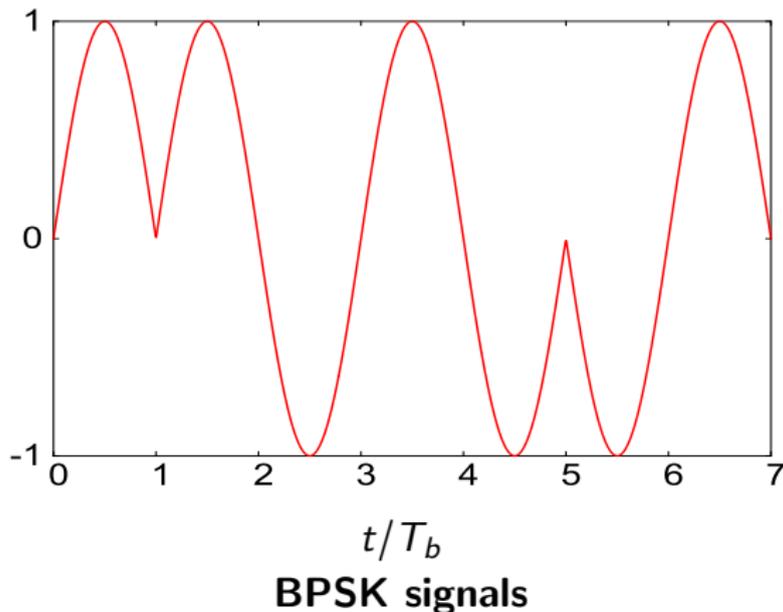
- Sampling at $t = kT$ and $y_k = \sum_{n=-\infty}^{\infty} I_n x_{k-n} + z_k$.

The transmission power is not $\|g(t) * c_\ell(t)\|^2$, which the receiver filter is to match! The additive interference to the transmitted information I_k is not just z_k but includes $\sum_{n=-\infty, n \neq k}^{\infty} I_n x_{k-n}$. So match filter is good for single transmission but may not be proper for consecutive transmissions!

Eye pattern

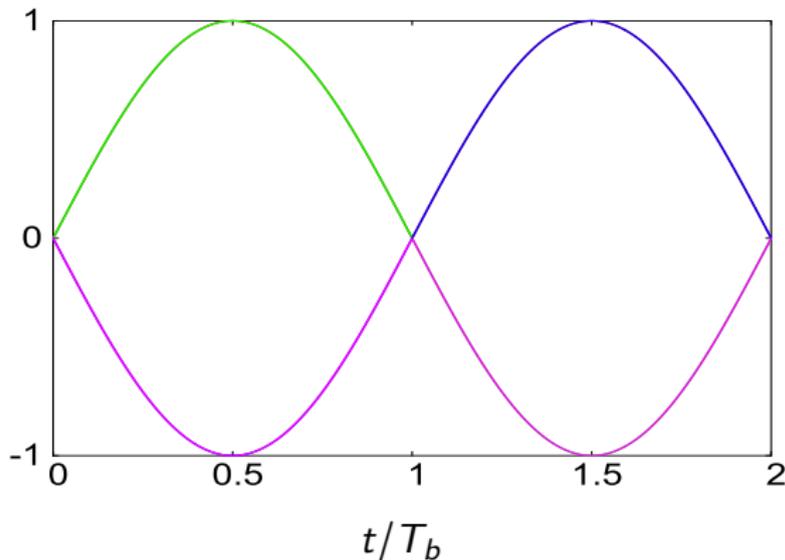
A good tool to examine **inter-symbol interference** is the **eye pattern**.

- Eye pattern: The synchronized superposition of all possible realizations of the signal of interest viewed within a particular signaling interval.



Perfect eye pattern (at Tx)

Eye pattern for $r_\ell(t)$ for $g(t)$ being half-cycle sine wave with duration T_b , $c_\ell(t) = \delta(t)$ and error-free BPSK transmission.



Now with $c_\ell(t) = \delta(t)$, we have, for example,

$$g(t) = \begin{cases} \frac{1}{\sqrt{T}}, & 0 \leq t < T \\ 0, & \text{otherwise} \end{cases} \quad (\text{Time-limited; hence, **band-unlimited!**})$$

$$h_\ell(t) = g(t) \star c_\ell(t) = g(t)$$

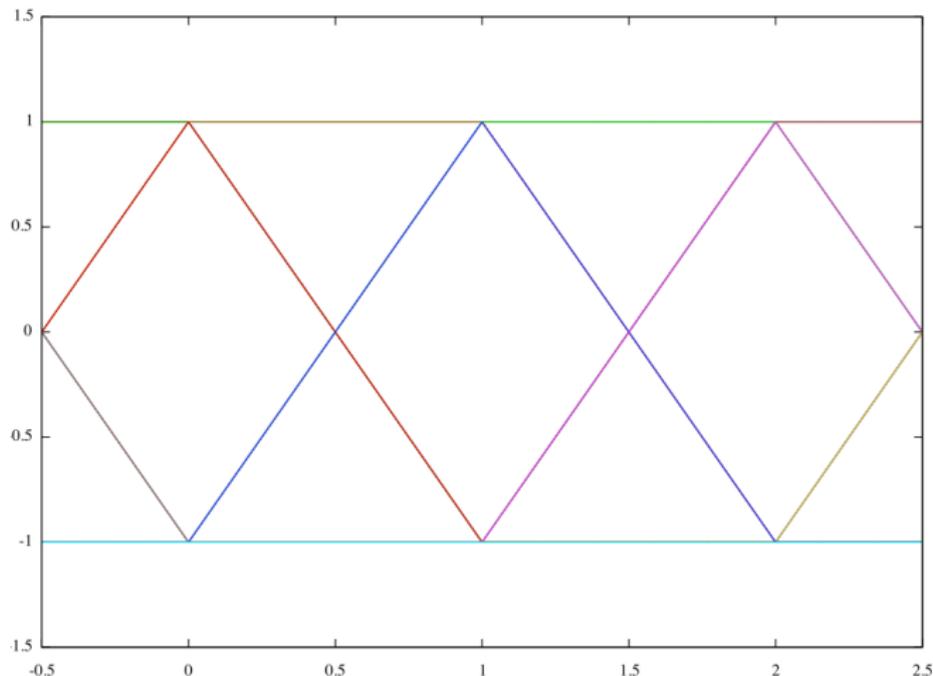
$$x_\ell(t) = h_\ell(t) \star h_\ell^*(-t) = \int_{-\infty}^{\infty} h_\ell(\tau) h_\ell^*(-(t-\tau)) d\tau$$

$$= \int_{-\infty}^{\infty} g(\tau) g(\tau-t) d\tau = \begin{cases} \frac{T-|t|}{T}, & |t| \leq T \\ 0, & \text{otherwise} \end{cases}$$

From here, you shall know the difference of using $h_\ell^*(T-t)$ and $h_\ell^*(-t)$, where the former samples at $t = T$, while the latter samples at $t = 0$.

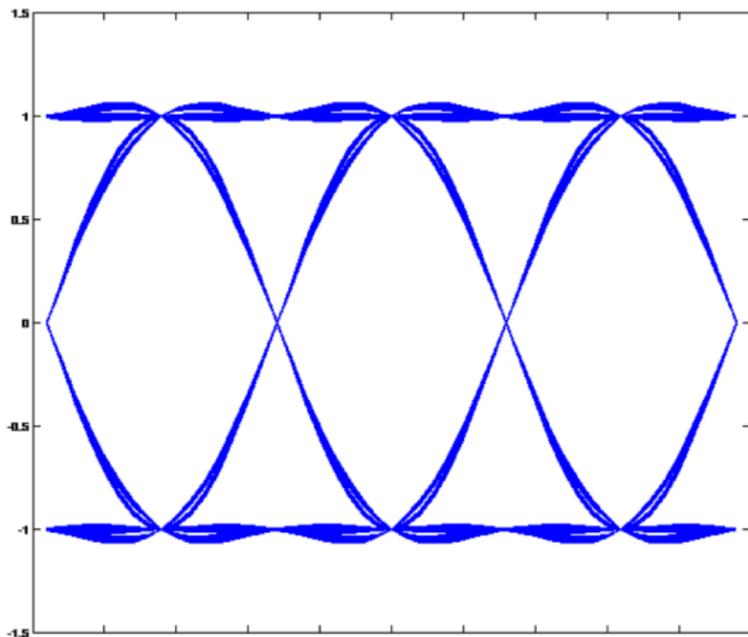
Perfect eye pattern (at Rx)

$y_\ell(t) = \sum_{n=-\infty}^{\infty} I_n x_\ell(t - nT)$ for all possible $\{I_n \in \{\pm 1\}\}_{n=-\infty}^{\infty}$.
($y_k = y_\ell(kT) = \sum_{n=-\infty}^{\infty} I_n x_\ell(kT - nT) = I_k$; so no ISI!)



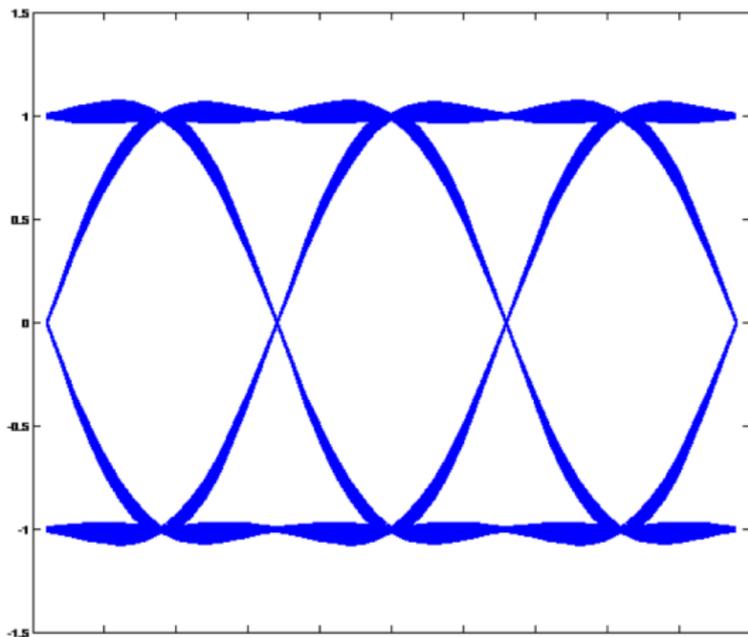
Example: BPSK with $1/T = 1K$ and $W = 3K$

Output $y_\ell(t)$ with $c_\ell(t)$ being ideal lowpass filter of bandwidth W .



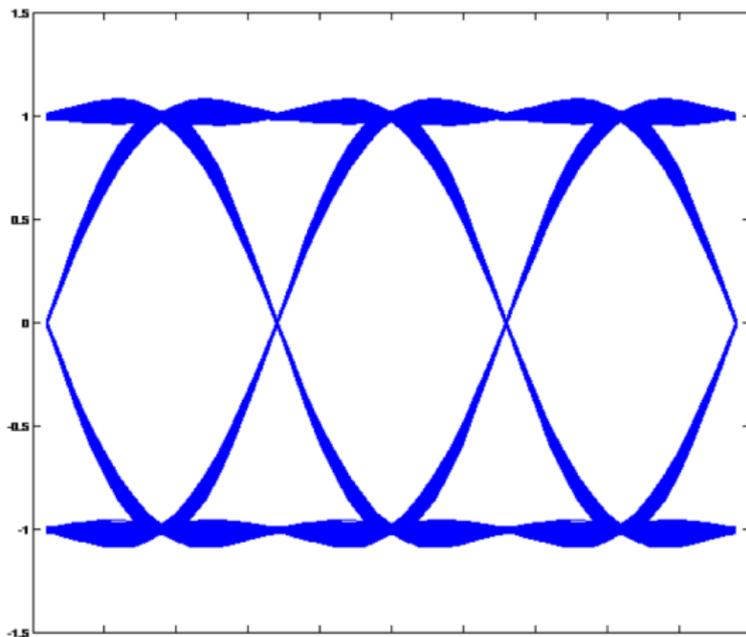
Example: BPSK with $1/T = 1K$ and $W = 1K$

Output $y_\ell(t)$ with $c_\ell(t)$ being ideal lowpass filter of bandwidth W .



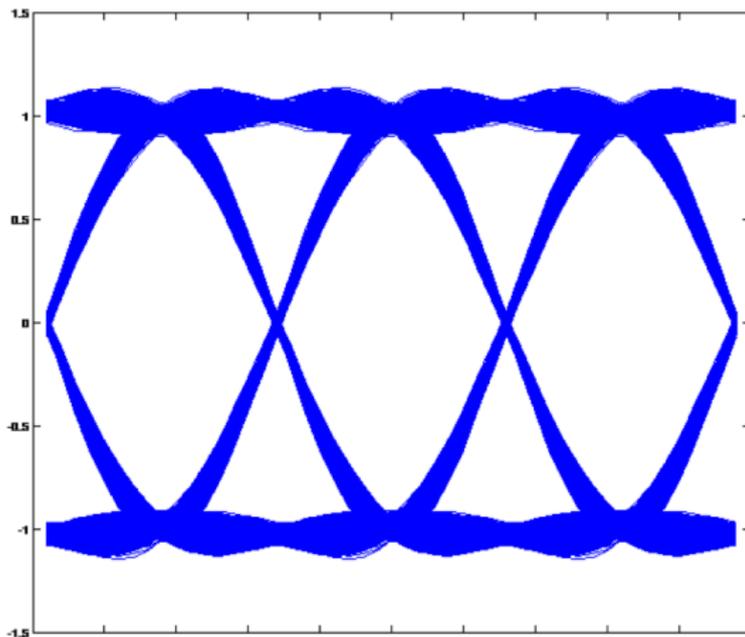
Example: BPSK with $1/T = 1K$ and $W = 0.9K$

Output $y_\ell(t)$ with $c_\ell(t)$ being ideal lowpass filter of bandwidth W .



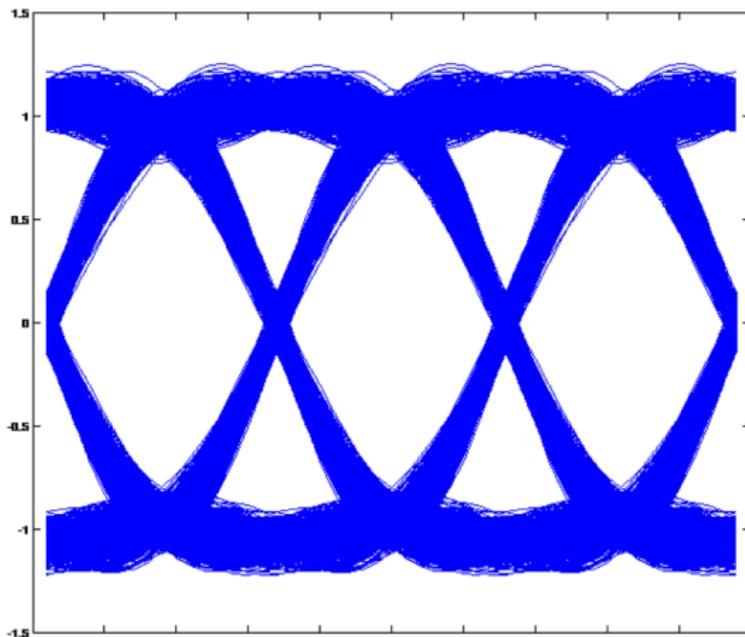
Example: BPSK with $1/T = 1K$ and $W = 0.8K$

Output $y_\ell(t)$ with $c_\ell(t)$ being ideal lowpass filter of bandwidth W .



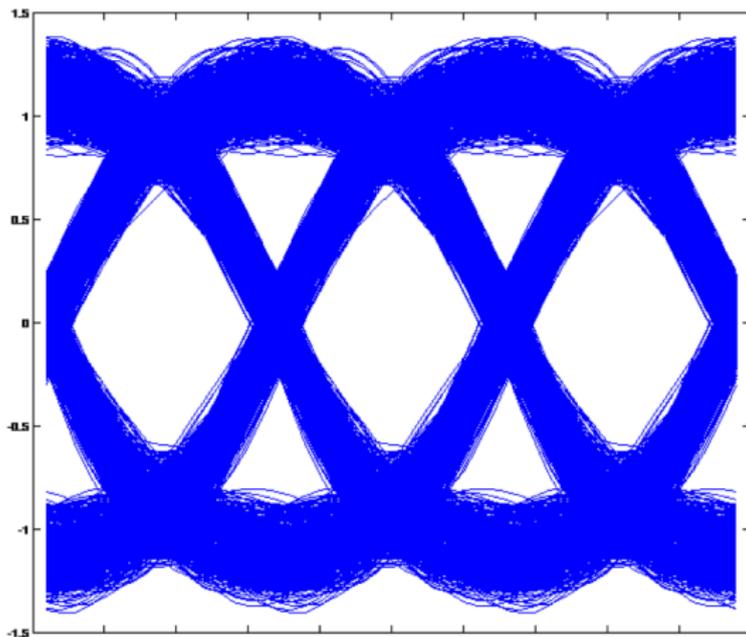
Example: BPSK with $1/T = 1K$ and $W = 0.7K$

Output $y_\ell(t)$ with $c_\ell(t)$ being ideal lowpass filter of bandwidth W .



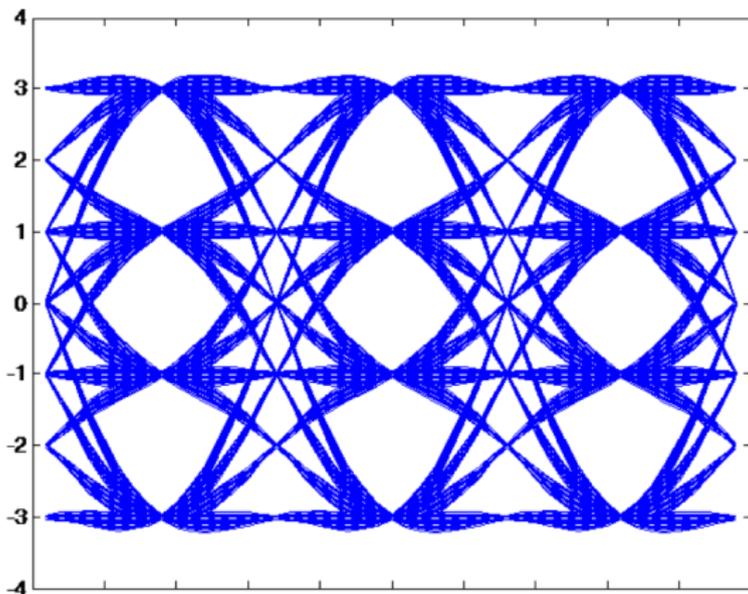
Example: BPSK with $1/T = 1K$ and $W = 0.6K$

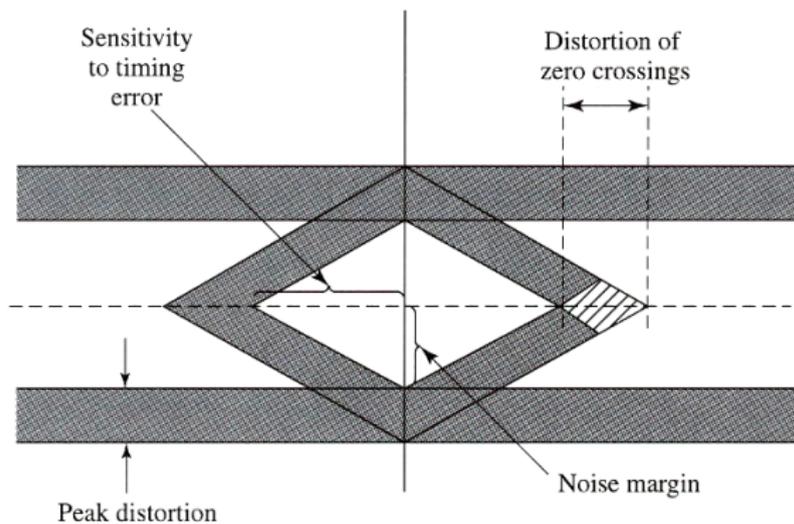
Output $y_\ell(t)$ with $c_\ell(t)$ being ideal lowpass filter of bandwidth W .



Example: 4PAM with $1/T = 1K$ and $W = 1K$

Output $y_\ell(t)$ with $c_\ell(t)$ being ideal lowpass filter of bandwidth W .





Conclusion: The smaller W

- Horizontal: Decision is more sensible to timing error.
- Vertical: Decision is more sensible to noise.

Example (revisited)

Now changing to $c_\ell(t) = \delta(t) + \delta(t - T)$, we have, for example,

$$g(t) = \begin{cases} \frac{1}{\sqrt{T}}, & 0 \leq t < T \\ 0, & \text{otherwise} \end{cases} \quad (\text{Time-limited; hence, **band-unlimited!**})$$

$$h_\ell(t) = g(t) * c_\ell(t) = g(t) + g(t - T) = g(t/2)$$

$$x_\ell(t) = h_\ell(t) * \underbrace{h_\ell^*(2T - t)}_{\text{causal}} = \int_{-\infty}^{\infty} h_\ell(\tau) h_\ell^*(2T - (t - \tau)) d\tau$$

$$= \int_{-\infty}^{\infty} g(\tau/2) g((2T + \tau - t)/2) d\tau$$

$$= \begin{cases} \frac{2T - |t - 2T|}{T}, & |t - 2T| \leq 2T \\ 0, & \text{otherwise} \end{cases}$$

$$y_k = y_\ell(kT) = \sum_{n=-\infty}^{\infty} I_n x_\ell(kT - nT) + z_\ell(kT) = 2I_{k-2} + \underbrace{I_{k-1} + I_{k-3}}_{\text{ISI}} + z_k$$

The question next to be asked is that how to remove the ISI?

9.2-1 Design of band-limited signals for no intersymbol interference - The Nyquist criterion

Intersymbol interference channel

$$y_k = \sum_{n=-\infty}^{\infty} I_n x_{k-n} + z_k$$

Design goal

Given W , T and $c_\ell(t)$, we would like to design $g(t)$ such that

$$x_{k-n} = \delta_{k-n}$$

and that

$$y_k = \sum_{n=-\infty}^{\infty} I_n x_{k-n} + z_k = I_k + z_k$$

Here, δ_k is the Kronecker delta function, defined as

$$\delta_k = \begin{cases} 1 & k = 0 \\ 0 & k \neq 0 \end{cases}.$$

Theorem 1 (Nyquist criterion)

Let $x_\ell(t)$ be a band-limited signal with band $[-W, W]$ and $x_\ell(0) = 1$. Sample at rate $\frac{1}{T}$ such that

$$x_k = x_\ell(kT) = \int_{-\infty}^{\infty} x_\ell(t) \delta(t - kT) dt = \delta_k$$

if and only if

$$\sum_{m=-\infty}^{\infty} X_\ell\left(f - \frac{m}{T}\right) = T$$

where $X_\ell(f) = \mathcal{F}\{x_\ell(t)\}$.

Proof:

The condition of $x_k = x_\ell(kT) = \delta_k$ is equivalent to

$$x_\ell(t) \sum_{k=-\infty}^{\infty} \delta(t - kT) = \sum_{k=-\infty}^{\infty} x_\ell(kT) \delta(t - kT) = \delta(t). \quad (1)$$

We however have (from Lemma 2 in the next slide)

$$\mathcal{F} \left\{ \sum_{k=-\infty}^{\infty} \delta(t - kT) \right\} = \frac{1}{T} \sum_{m=-\infty}^{\infty} \delta \left(f - \frac{m}{T} \right) \text{ and } \mathcal{F} \{ \delta(t) \} = 1.$$

Taking Fourier transform on both sides of (1) gives

$$X_\ell(f) * \left[\frac{1}{T} \sum_{m=-\infty}^{\infty} \delta \left(f - \frac{m}{T} \right) \right] = \frac{1}{T} \sum_{m=-\infty}^{\infty} X_\ell \left(f - \frac{m}{T} \right) = 1,$$

and proves the theorem. □

Proof of key lemma

Lemma 2

$$\mathcal{F} \left\{ \sum_{k=-\infty}^{\infty} \delta(t - kT) \right\} = \frac{1}{T} \sum_{m=-\infty}^{\infty} \delta \left(f - \frac{m}{T} \right)$$

Proof: Consider the function

$$\alpha(f) = \frac{1}{T} \sum_{m=-\infty}^{\infty} \delta \left(f - \frac{m}{T} \right)$$

which is periodic with period $\frac{1}{T}$. From Fourier series, we have

$$\alpha(f) = \frac{1}{1/T} \sum_{n=-\infty}^{\infty} c_n e^{-j2\pi n f / (1/T)} = \sum_{n=-\infty}^{\infty} e^{-j2\pi n f T}$$

where

$$c_n = \int_{-\frac{1}{2T}}^{\frac{1}{2T}} \alpha(f) e^{j2\pi n f / (1/T)} df = \int_{-\frac{1}{2T}}^{\frac{1}{2T}} \frac{1}{T} \delta(f) e^{j2\pi n f / (1/T)} df = \frac{1}{T}$$

by following the replication property of $\delta(f)$.

Next by linearity of Fourier transform, we have

$$\begin{aligned}\mathcal{F}\left\{\sum_{k=-\infty}^{\infty}\delta(t-kT)\right\} &= \int_{-\infty}^{\infty}\sum_{k=-\infty}^{\infty}\delta(t-kT)e^{-j2\pi ft}dt \\ &= \sum_{k=-\infty}^{\infty}e^{-j2\pi fkT}.\end{aligned}$$



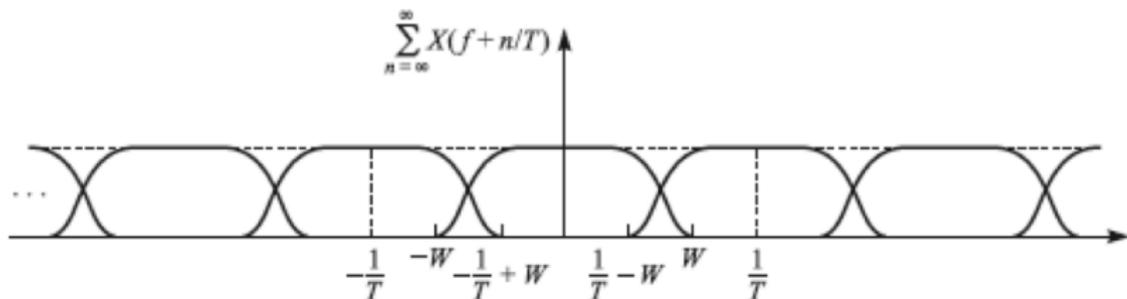
Implication of Nyquist criterion

$$x_k = \delta_k \quad \text{iff} \quad \sum_{m=-\infty}^{\infty} X_\ell \left(f - \frac{m}{T} \right) = T \quad (2)$$

- 1 $2W < \frac{1}{T}$:
 $X_\ell \left(f - \frac{m}{T} \right)$ and $X_\ell \left(f - \frac{m'}{T} \right)$ do not overlap for $m \neq m'$.
Hence (2) is impossible!
- 2 $2W = \frac{1}{T}$:
This means $X_\ell(f) = T \text{rect}(Tf)$, hence $x_\ell(t) = \text{sinc}\left(\frac{t}{T}\right)$.
Theoretically ok but physically impossible!
- 3 So we need $2W > \frac{1}{T}$

Channel bandwidth must be larger than **sampling rate**.

$$x_k = \delta_k \quad \text{iff} \quad \sum_{m=-\infty}^{\infty} X_l \left(f - \frac{m}{T} \right) = T$$



$$2W > \frac{1}{T} \quad \left(\text{from } W > \frac{1}{T} - W \right)$$

Raised cosine pulse

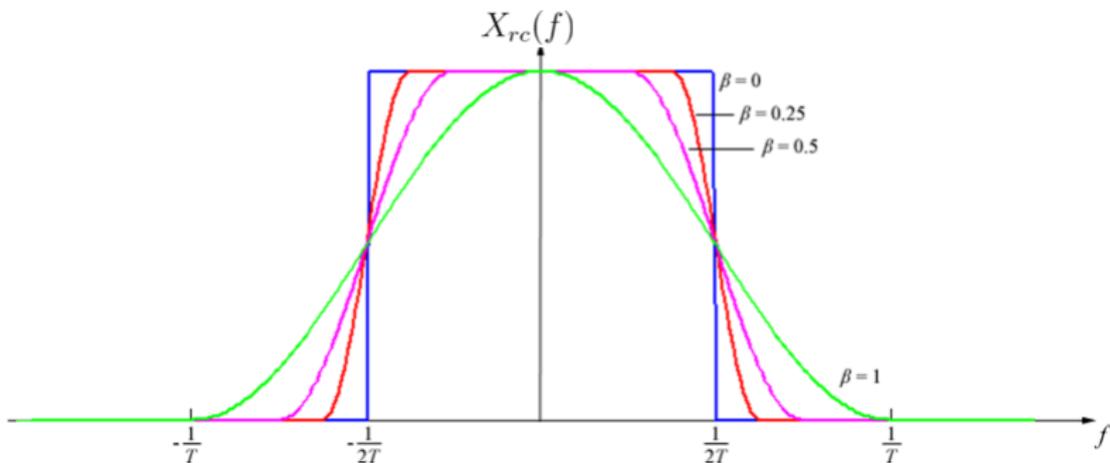
Definition 1

$$X_{rc}(f) = \begin{cases} T, & 0 \leq |f| \leq \frac{1-\beta}{2T} \\ \frac{T}{2} \left\{ 1 + \cos \left[\frac{\pi T}{\beta} \left(|f| - \frac{1-\beta}{2T} \right) \right] \right\}, & \frac{1-\beta}{2T} \leq |f| \leq \frac{1+\beta}{2T} \\ 0, & \text{otherwise} \end{cases}$$

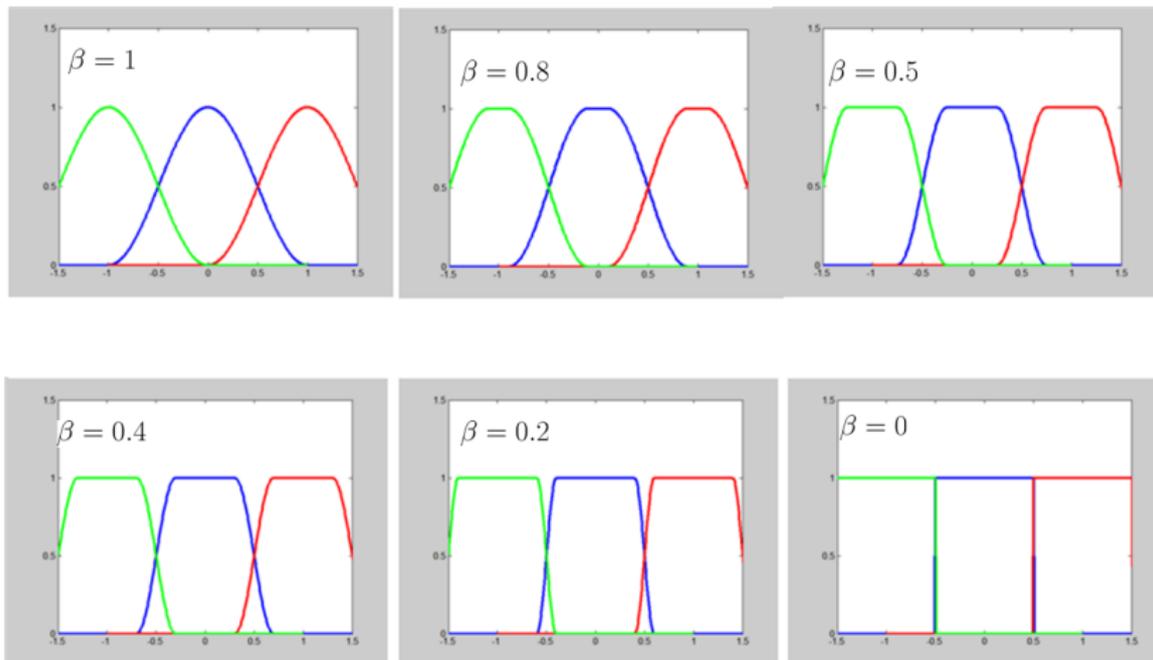
where $0 \leq \beta \leq 1$ is the roll-off factor.

$$x_{rc}(t) = \text{sinc} \left(\frac{t}{T} \right) \frac{\cos(\pi\beta t/T)}{1 - 4\beta^2 t^2/T^2}$$

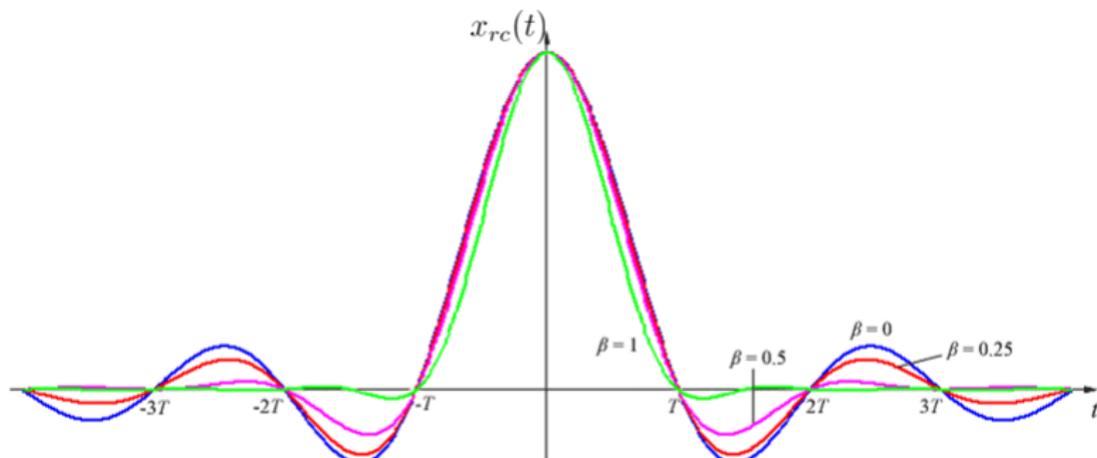
$$X_{rc}(f) = \begin{cases} T, & 0 \leq |f| \leq \frac{1-\beta}{2T} \\ \frac{T}{2} \left\{ 1 + \cos \left[\frac{\pi T}{\beta} \left(|f| - \frac{1-\beta}{2T} \right) \right] \right\}, & \frac{1-\beta}{2T} \leq |f| \leq \frac{1+\beta}{2T} \\ 0, & \text{otherwise} \end{cases}$$



$$X_{rc}\left(f - \frac{m}{T}\right) \text{ with } m = -1, 0, 1$$



$$x_{rc}(t) = \text{sinc}\left(\frac{t}{T}\right) \frac{\cos(\pi\beta t/T)}{1 - 4\beta^2 t^2/T^2}$$



Example.

Assuming

$$C_\ell(f) = 1$$

- Let $G_T(f) = \mathcal{F}\{g(t)\}$.
- Let $G_R(f) = \mathcal{F}\{h_\ell^*(-t)\}$, where $h_\ell(t) = g(t) * c_\ell(t) = g(t)$.

This gives

$$G_R(f) = \mathcal{F}\{g^*(-t)\} = G_T^*(f)$$

and

$$X_{rc}(f) = G_T(f)C_\ell(f)G_R(f) = G_T(f)G_R(f) = |G_T(f)|^2.$$

- Note $|x_{rc}(t)| \approx \frac{1}{t^3}$ for large $|t|$. So it can be truncated at $\pm t_0$ for some t_0 large.

$$x_{rc}(t) = \text{sinc}\left(\frac{t}{T}\right) \frac{\cos(\pi\beta t/T)}{1 - 4\beta^2 t^2/T^2}$$

So we can set

$$G_T(f) = \sqrt{X_{rc}(f)} e^{-i2\pi ft_0} \quad \text{and} \quad G_R(f) = G_T^*(f).$$

9.2-2 Design of band-limited signals with controlled ISI: Partial response signals

Duobinary pulse

We relax the no-ISI condition so that

$$x_k = \delta_k + \delta_{k-1} \implies y_k = I_k + I_{k-1} + z_k$$

Following similar arguments (see the next slide), it shows

$$\frac{1}{T} \sum_{m=-\infty}^{\infty} X_\ell \left(f - \frac{m}{T} \right) = 1 + e^{-j2\pi fT}.$$

Setting $2W = \frac{1}{T}$ (with W being the bandwidth of $X_\ell(f)$), we have

$$\begin{aligned} X_\ell(f) &= T \left(1 + e^{-j2\pi fT} \right) \text{rect} \left(\frac{f}{2W} \right) \\ x_\ell(t) &= \text{sinc}(2Wt) + \text{sinc} \left[2 \left(Wt - \frac{1}{2} \right) \right] \end{aligned}$$

This is called **duobinary pulse**.

Proof: The condition of $x_k = \delta_k + \delta_{k-1}$ is equivalent to

$$x_\ell(t) \sum_{k=-\infty}^{\infty} \delta(t-kT) = \sum_{k=-\infty}^{\infty} x_\ell(kT)\delta(t-kT) = \delta(t) + \delta(t-T). \quad (3)$$

We however have

$$\mathcal{F} \left\{ \sum_{k=-\infty}^{\infty} \delta(t-kT) \right\} = \frac{1}{T} \sum_{m=-\infty}^{\infty} \delta \left(f - \frac{m}{T} \right) \text{ and } \mathcal{F} \{ \delta(t) \} = 1.$$

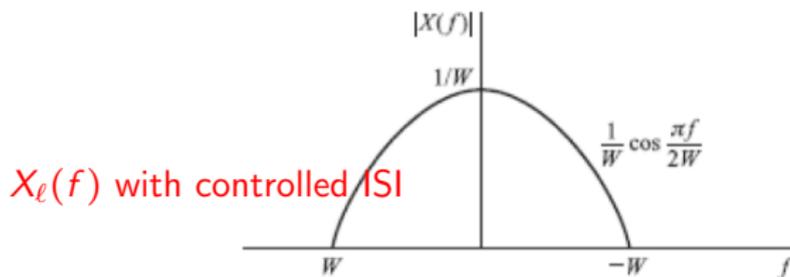
Taking Fourier transform on both sides of (3) gives

$$X_\ell(f) \star \left[\frac{1}{T} \sum_{m=-\infty}^{\infty} \delta \left(f - \frac{m}{T} \right) \right] = \frac{1}{T} \sum_{m=-\infty}^{\infty} X_\ell \left(f - \frac{m}{T} \right) = 1 + e^{-j2\pi fT},$$

and proves the theorem.

When $W = \frac{1}{2T}$,

$$X_{\ell}(f) = \begin{cases} T(1 + e^{-j2\pi fT}) \operatorname{rect}\left(\frac{f}{2W}\right), & \text{with controlled ISI} \\ T \operatorname{rect}\left(\frac{f}{2W}\right), & \text{without controlled ISI} \end{cases}$$



The duobinary filter is apparently more physically realizable!

Recall that with no controlled ISI, we require $W > \frac{1}{2T}$ because channel bandwidth $W = \frac{1}{2T}$ is not physically realizable. But now with controlled ISI, $W = \frac{1}{2T}$ becomes physically realizable.

9.2-3 Data detection for controlled ISI

Precoding for duobinary pulses

Received signal for duobinary shaping is

$$y_k = I_k + I_{k-1} + z_k.$$

We could **precode** the sequence $\{I_k\}$ to simplify detection.

Example 1 (Binary case - Differential encoding)

Given the binary bit (information) stream $\{b_k\}$

- Define $P_k = b_k \oplus P_{k-1} \in \{0, 1\}$.
- Set $I_k = 2P_k - 1 \in \{\pm 1\}$.
- Receive $y_k = I_k + I_{k-1} + z_k$.

$$I_k + I_{k-1} = \begin{cases} \pm 2, & \text{if } b_k = 0 \\ 0, & \text{if } b_k = 1. \end{cases}$$

- $\hat{b}_k = 0$ if $|y_k| > 1$ and $\hat{b}_k = 1$ if $|y_k| \leq 1$

Summary of precoding system

$$\text{Compare } \begin{cases} \frac{1}{T} \sum_{m=-\infty}^{\infty} X_{\ell}(f - \frac{m}{T}) = 1 \\ \frac{1}{T} \sum_{m=-\infty}^{\infty} X_{\ell}^{(p)}(f - \frac{m}{T}) = 1 + e^{-j2\pi fT} \end{cases}$$

We can say $X_{\ell}^{(p)}(f) = X_{\ell}(f)(1 + e^{-j2\pi fT})$ and

$$\begin{cases} y_{\ell}(t) = \sum_{n=-\infty}^{\infty} I_n X_{\ell}(t - nT) + z_{\ell}(t) \\ y_{\ell}^{(p)}(t) = \sum_{n=-\infty}^{\infty} I_n X_{\ell}^{(p)}(t - nT) + z_{\ell}(t) \end{cases}$$

and

$$\begin{cases} y_k = I_k + z_k \\ y_k^{(p)} = I_k + I_{k-1} + z_k \end{cases} \Rightarrow \begin{cases} y_k \leq 0 \\ |y_k^{(p)}| \leq 1 \end{cases}$$

Note that $\|x_{\ell}(t)\|^2$ does not decide the transmission energy!

Summary of precoding system

$$\Rightarrow \begin{cases} P_e = Q\left(\sqrt{\frac{1}{\mathbb{E}[z_k^2]}}\right) = Q\left(\sqrt{\frac{\mathcal{E}_{b,\ell}/\|g_T(t)\|^2}{N_0\|g_R(t)\|^2}}\right), & \text{error rate for } l_k \\ = Q\left(\sqrt{\frac{2\mathcal{E}_b}{N_0} \frac{1}{\|g_T(t)\|^2\|g_R(t)\|^2}}\right) = Q(\sqrt{2a\gamma_b}) \\ P_e^{(p)} = \frac{3}{2}Q(\sqrt{2a\gamma_b}) - \frac{1}{2}Q(3\sqrt{2a\gamma_b}), & \text{error rate for } b_k \end{cases}$$

where

$$\left\{ \begin{array}{l} l_k \in \{\pm 1\} \\ \text{the (lowpass) transmission energy per bit } \mathcal{E}_{b,\ell} = \|g_T(t)\|^2 = 2\mathcal{E}_b \\ \text{the lowpass noise } \mathbb{E}[z_k^2] = \sigma_\ell^2 \|g_R(t)\|^2 \\ \quad \text{with } n_\ell(t) \text{ having two-sided PSD } \sigma_\ell^2 = N_0 \\ a = \frac{1}{\|g_T(t)\|^2\|g_R(t)\|^2} \text{ (subject to } g_T(t) * c_\ell(t) * g_R(t) = x_\ell(t)) \end{array} \right.$$

Hence, pre-coding technique provides a better spectrum efficiency at the price of performance degradation.

9.2-4 Signal design for channel with distortion

In general, we have $C_\ell(f) \neq \text{rect}\left(\frac{f}{2W}\right)$, and in this case

$$s_\ell(t) = \sum_{n=-\infty}^{\infty} I_n g_T(t - nT)$$

$$r_\ell(t) = c_\ell(t) * s_\ell(t) + n_\ell(t)$$

$$y_\ell(t) = r_\ell(t) * g_R(t) = s_\ell(t) * c_\ell(t) * g_R(t) + z_\ell(t)$$

$$y_k = y_\ell(kT) = I_k + z_k \quad (\text{We hope there is no ISI!})$$

where

- $g_T(t)$ transmit filter
- $c_\ell(t)$ channel impulse response
- $g_R(t)$ receive filter

Hence

$$\begin{cases} X_{rc}(t) = g_T(t) * c_\ell(t) * g_R(t) \\ X_{rc}(f) = G_T(f) C_\ell(f) G_R(f) \\ S_{z_\ell}(f) = N_0 |G_R(f)|^2 \text{ because we assume } \{I_k\} \text{ real} \end{cases}$$

If $c_\ell(t)$ is known to Tx, then we may choose to “pre-equalize” the channel effect at Tx:

$$|G_T(f)| = \frac{\sqrt{X_{rc}(f)}}{|C_\ell(f)|} \quad \text{and} \quad |G_R(f)| = \sqrt{X_{rc}(f)}$$

Then, ISI is avoided; also, the noise power remains

$$\mathbb{E}[z_k^2] = \int_{-\infty}^{\infty} \underbrace{S_{z_\ell}(f)}_{=N_0|G_R(f)|^2} df = N_0 \int_{-\infty}^{\infty} X_{rc}(f) df = N_0 X_{rc}(0) = N_0.$$

$$I_n \in \{\pm d\} \text{ and } X_{rc}(f) = G_T(f)C_\ell(f)G_R(f)$$

Signal power

$$P_{av,\ell} = \frac{d^2 \|g_T(t)\|^2}{T} = \frac{d^2}{T} \int_{-\infty}^{\infty} \frac{X_{rc}(f)}{|C_\ell(f)|^2} df$$

Error probability

$$\begin{aligned} P_b &= Q\left(\sqrt{\frac{d_{12}^2}{4\mathbb{E}[z_k^2]}}\right) \\ &= Q\left(\frac{d}{\sqrt{\mathbb{E}[z_k^2]}}\right) = Q\left(\sqrt{\frac{P_{av,\ell} T}{N_0 \left[\int_{-\infty}^{\infty} \frac{X_{rc}(f)}{|C_\ell(f)|^2} df\right]}}\right) \end{aligned}$$

If $c_\ell(t)$ only known to Rx

We can only equalize the “channel effect” at Rx:

$$|G_T(f)| = \sqrt{X_{rc}(f)} \quad \text{and} \quad |G_R(f)| = \frac{\sqrt{X_{rc}(f)}}{|C_\ell(f)|}.$$

Signal power

$$P_{av,\ell} = \frac{d^2}{T} \|g_T(t)\|^2 = \frac{d^2}{T} \int_{-\infty}^{\infty} X_{rc}(f) df = \frac{d^2}{T}$$

Noise power

$$\mathbb{E}[z_k^2] = \int_{-\infty}^{\infty} S_{z_\ell}(f) df = N_0 \int_{-\infty}^{\infty} \frac{X_{rc}(f)}{|C_\ell(f)|^2} df$$

Error probability

$$P_b = Q\left(\frac{d}{\sqrt{\mathbb{E}[z_k^2]}}\right) = Q\left(\sqrt{\frac{P_{av,\ell} T}{N_0 \left[\int_{-\infty}^{\infty} \frac{X_{rc}(f)}{|C_\ell(f)|^2} df\right]}}\right)$$

If however $c_\ell(t)$ known to both Tx and Rx

We may design:

$$|G_T(f)| = \sqrt{\frac{X_{rc}(f)}{|C_\ell(f)|}} \quad \text{and} \quad |G_R(f)| = \sqrt{\frac{X_{rc}(f)}{|C_\ell(f)|}}$$

Signal power

$$P_{av,\ell} = \frac{d^2}{T} \|g_T(t)\|^2 = \frac{d^2}{T} \int_{-\infty}^{\infty} \frac{X_{rc}(f)}{|C_\ell(f)|} df$$

Noise power

$$\mathbb{E}[z_k^2] = \int_{-\infty}^{\infty} S_{z_\ell}(f) df = N_0 \int_{-\infty}^{\infty} \frac{X_{rc}(f)}{|C_\ell(f)|} df$$

Error probability

$$P_b = Q\left(\frac{d}{\sqrt{\mathbb{E}[z_k^2]}}\right) = Q\left(\sqrt{\frac{P_{av,\ell} T}{N_0 \left[\int_{-\infty}^{\infty} \frac{X_{rc}(f)}{|C_\ell(f)|} df\right]^2}}\right)$$

Either Tx or Rx knows $c_\ell(t)$

$$P_{b,T} = P_{b,R} = Q \left(\sqrt{\frac{P_{av,\ell} T}{N_0 \left[\int_{-\infty}^{\infty} \frac{X_{rc}(f)}{|C_\ell(f)|^2} df \right]}} \right)$$

Both Tx and Rx know $c_\ell(t)$

$$P_{b,TR} = Q \left(\sqrt{\frac{P_{av,\ell} T}{N_0 \left[\int_{-\infty}^{\infty} \frac{X_{rc}(f)}{|C_\ell(f)|} df \right]^2}} \right)$$

Note from Cauchy-Schwartz inequality

$$\begin{aligned} \left[\int_{-\infty}^{\infty} \frac{X_{rc}(f)}{|C_\ell(f)|} df \right]^2 &= \left\| \left\langle \sqrt{X_{rc}(f)}, \frac{\sqrt{X_{rc}(f)}}{|C_\ell(f)|} \right\rangle \right\|^2 \\ &\leq \left\| \sqrt{X_{rc}(f)} \right\|^2 \left\| \frac{\sqrt{X_{rc}(f)}}{|C_\ell(f)|} \right\|^2 = \int_{-\infty}^{\infty} \frac{X_{rc}(f)}{|C_\ell(f)|^2} df \end{aligned}$$

This shows $P_{b,TR} \leq P_{b,T} = P_{b,R}$. “=” holds iff $|C_\ell(f)| = 1$.

What you learn from Chapter 9



- Match filter to input pulse shaping and channel impulse response
 - (Good to know) Eye pattern to examine ISI
- Nyquist criterion
 - Sampling rate $<$ channel bandwidth for no ISI (i.e., increasing sampling rate will give more samples for perhaps better performance, but adjacent samples will be eventually “interfered” to each other)
 - Since ISI is unavoidable for high sampling rate, let’s accept and face it, and just use **controlled ISI**.
- A better performance is resulted when both Tx and Rx know the channel.